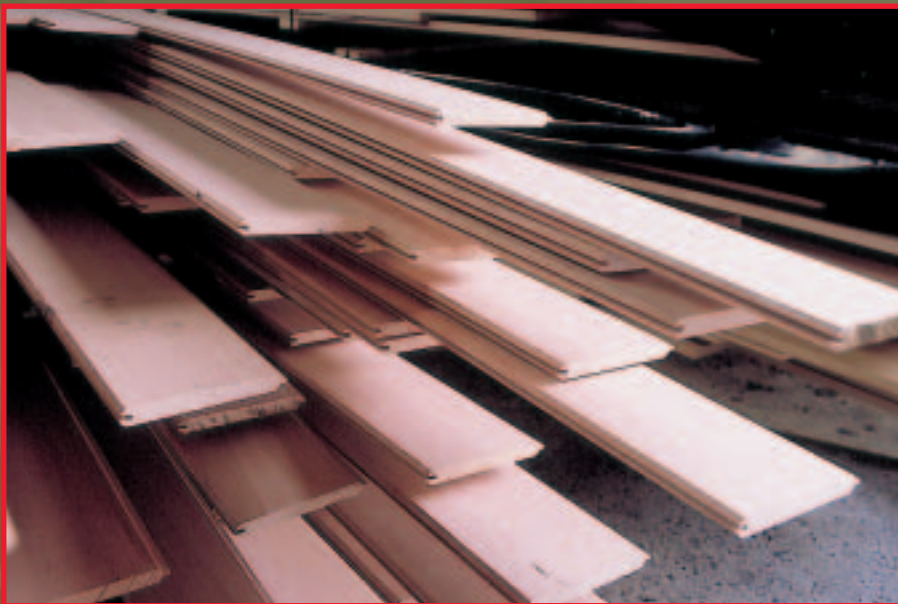




**Australian Government**

**Forest and Wood Products  
Research and Development  
Corporation**

# **Moisture variation in dried hardwood timber**





© 2004 Forest & Wood Products Research & Development Corporation  
All rights reserved.

***Publication: Moisture Variation in Dried Hardwood Timber***

The Forest and Wood Products Research and Development Corporation ("FWPRDC") makes no warranties or assurances with respect to this publication including merchantability, fitness for purpose or otherwise. FWPRDC and all persons associated with it exclude all liability (including liability for negligence) in relation to any opinion, advice or information contained in this publication or for any consequences arising from the use of such opinion, advice or information.

This work is copyright and protected under the Copyright Act 1968 (Cth). All material except the FWPRDC logo may be reproduced in whole or in part, provided that it is not sold or used for commercial benefit and its source (Forest and Wood Products Research and Development Corporation) is acknowledged. Reproduction or copying for other purposes, which is strictly reserved only for the owner or licensee of copyright under the Copyright Act, is prohibited without the prior written consent of the Forest and Wood Products Research and Development Corporation.

***Project no: PN01.1305***

***Researchers:***

A. Redman  
Formerly: **QFRI - Processing & Utilisation**  
Queensland Forestry Research Institute  
GPO Box 46, Brisbane, Qld 4001

Currently: **CSIRO Forestry and Forest Products**  
Private Bag 10, Clayton South, VIC 3169

**Forest and Wood Products Research and Development Corporation**

PO Box 69, World Trade Centre, Victoria 8005  
Phone: 03 9614 7544 Fax: 03 9614 6822 Email: [info@fwprdc.org.au](mailto:info@fwprdc.org.au)  
Web: [www.fwprdc.org.au](http://www.fwprdc.org.au)

# **Moisture Variation in Dried Hardwood Timber**

Prepared for the

**Forest & Wood Products  
Research & Development Corporation**

by

**A. Redman**

*The FWPRDC is jointly funded by the Australian forest and wood products industry  
and the Australian Government.*

## Introduction

This was a joint project of the Timber Research Unit (TRU) of the University of Tasmania and the Queensland Forest Research Institute (QFRI). It was supported by the Tasmanian Forests and Forest Industry Council (FFIC), and many of Australia's major hardwood producers including Hume and Kerrison, Hyne & Son, Clennett Timbers, Hurfords Hardwoods and J. Notaras & Sons.

This project was nominated by the Australian hardwood timber industry and therefore demonstrates that the desired outcomes should be directly beneficial to this sector. The focus of the Australian hardwood timber industry is currently moving from producing predominantly structural grade products to appearance grade products. This is due to increased demand for appearance grade timber for products such as flooring and furniture, increasing competition in the structural timber market from softwoods and non-timber products and expanding export markets.

The objectives of this project were to:

1. Understand why moisture gradients occur in Australian hardwoods during drying and their affects on the performance of timber in service;
2. Improve existing technology(ies) and/or processes to reduce moisture content (MC) variability between and within boards during drying of Australian hardwoods in an economical and practical manner.

The equilibrium moisture content (EMC) tolerances for appearance grade timbers are more demanding than those for structural grade timbers due to performance requirements, as is reflected in the grade quality requirements. Varying MC within and between pieces leads to problems in timber utilisation, mainly through shrinkage and instability. Eucalypts are regarded as being notorious for exhibiting problems with MC variation and this problem is a significant threat to the successful marketing of Australian hardwoods in markets such as flooring, joinery and furniture. Additionally, problems with MC variation are regarded as a serious impediment to the drying of hardwoods.

Anecdotally it is reported that the problems are more pronounced in younger plantation and regrowth material. Increasing pressure to produce appearance grade products, where there is reduced tolerance of moisture variation in the relevant standards, compounds the problem. As a direct result of this, the increased incidence of MC related problems in the marketplace has in turn led to an increase in the number of consumer claims against timber processors. Additionally, moisture variation in hardwood timber during drying increases production costs because of the longer kiln drying time required to produce more uniformly dried timber.

Therefore, the importance of identifying problematic species, establishing causal factors and their affect on service performance and investigation of potential economically viable solutions would be of great benefit to the current hardwood timber industry.

Originally this project had a two-year time span. However due to the unexpected nature of the results obtained the project has been terminated, after approximately one year, under unanimous agreement between FWPRDC, QFRI, TRU and other industry collaborators. The section of research covered in this document involves an intensive case study by QFRI at Hurfords Building Supplies Pty. Ltd. (NSW) to identify the cause of MC variation and its effect on the performance of timber in service. Additionally, dry stock appraisal studies were performed at Clennett Timber, Hume and Kerrison, Hurfords Building Supplies, Hyne & Son and J. Notaras & Sons mills.

## Executive Summary

This project comprised two parts. The first involved an extensive study conducted at Hurfords Building Supplies sawmill to investigate the cause of the moisture variation problem. The second concerned the determination of the extent of the problem's occurrence through appraisals of randomly selected dried stock at various industrial hardwood sawmills.

The case study at Hurfords Building Supplies was performed predominately to examine appropriate variables of regrowth spotted gum (*E. maculata*) from the harvest site to the final dried product in order to obtain problematic material and thus establish the cause of the problem. The variables examined in this study were: coupe location; board location within a log; moisture content (MC) of boards before and after pre-drying; location of board within a stack; kiln airflow and temperature distribution during drying; and board length and sawn (growth ring) orientation. Each variable was considered a potential cause of the moisture variation problem. They were measured with the premise of determining if a correlation exists between any of the variables, and the final MC of problematic material selected at the end of the trial.

Initially, approximately 1350 100 × 25mm (nominal dimension) were sawn from a selection of logs from 4 different coupes. Approximately half of the boards contained templates adhered to their ends to identify their within log position. The boards were racked and left in the air-drying yard to dry to an average MC of 19%. The timber is usually dried to a lower average MC but it was believed that this higher MC would exacerbate the variation problem. The material was then kiln dried. Temperature and airflow tests at the stack face proved to be stable with little variation. After kiln drying and equalising to a target MC of 11%, the MC of each board was tested using a resistance type moisture meter.

Results at this stage revealed that MC values for the entire set of boards ranged from 8% to 16%. The 50 wettest, 50 driest and 50 boards with MCs closest to the target (control boards) were selected and tested for MC at 500mm intervals using the more accurate oven dry method (in accordance with AS/NZS 1080.1). This revealed the MC variation of the selected material to be even less, ranging from 9.2% to 12.8%. For the number of boards and associated variables used in this study these results, did not produce any problematic moisture variable material to be used for further research.

This second part of this project involved dry stock appraisals conducted at, Clennett Timber (Tas), Hume and Kerrison Pty. Ltd. (Tas), Hurfords Building Supplies Pty. Ltd. (NSW), J. Notaras & Sons Pty. Ltd. (NSW), Hyne & Son Pty. Ltd. (QLD). The two highest output volume species of timber were appraised for each sawmill, concentrating on high grade joinery and flooring material. The species investigated were *E. delegatensis*, *E. pilularis*, *E. regnans*, and *Corymbia maculata*.

The appraisals themselves involved measurements of both average MC and MC gradient from a subset (in accordance with AS/NZ 4787). Results from the dry stock appraisals indicated that a moisture variation problem did exist. Additionally, further questions have been raised relating drying practice to the problem, indicating that timber properties are not necessarily the underlining cause as initially believed.

As the results obtained from the mill study section of this research prevented further investigations, through consensus from the industry stakeholders, FWPRDC, University of Tasmania and QFRI, the project was terminated after approximately one year. The results from this study have however, broadened our knowledge of the moisture variation and have changed the scope for further investigations into the problem.

# Contents

Introduction		i
Executive Summary		ii
Chapter 1.	Literature Review	1
Chapter 2.	Sawmill Study	9
Chapter 3.	Dry Stock Appraisals	22
Recommendations for Further Work		26
References.		28
Appendix A.	Survey Meeting Minutes – Hurfords	30
Appendix B.	Mill Study Data	31
Appendix C	Dry Stock Appraisal Data	51

## Chapter 1. Literature Review

The objective of timber drying, simply stated, is to remove moisture from a board as quickly as possible without an unacceptable amount of degrade. Inherent in the terms “moisture removal” is the concept of changing the moisture level from some initial, often variable, value to a lower level or range that is dictated by either standards or customer requirements. Generally, this end point moisture content value is specified to be within a certain range of values and is dictated by the atmospheric conditions of the end use location so that it is close to the equilibrium moisture content of the timber. Occasionally, problematic boards occur after drying which are wetter or drier than the average and which are not believed to be due to drying practices. Thus, a review of previous literature was conducted to explore potential reasons for the occurrence of this phenomenon.

### Equilibrium Moisture Content (EMC) & EMC Charts

The equilibrium moisture content (EMC) of timber is the moisture content (MC), at which the timber neither gains nor loses moisture from the surrounding atmosphere. The EMC varies to some extent with seasonal changes and, for practical purposes, an EMC range is normally quoted for a particular locality. Subsequent shrinkage or expansion will be minimal when timber is used at a MC within the quoted EMC range (McNaught, 1987).

The atmospheric variables that affect the EMC of timber include: the surrounding temperature, relative humidity (RH) and atmospheric pressure. Of these, the one that has by far the largest influence is RH. RH is defined as a measure of the amount of water vapour in the air at any particular temperature, expressed as a percentage of the vapour that can be carried by the air when it is saturated at that temperature.

The term isotherm is defined as a graphical line or map connecting temperature to other variables. This data is often presented as a chart or table made up of a number of isotherms relating dry bulb temperature, wet bulb depression, RH and corresponding EMC values. The chart most commonly used in the timber industry in Australia was created by CSIRO and is presented in figure 1.1. It is also reproduced in Waterson (1997).

This chart has significant importance for the timber industry in terms of creating drying schedules and determining the best conditions to give end point MCs corresponding to atmospheric EMC conditions.

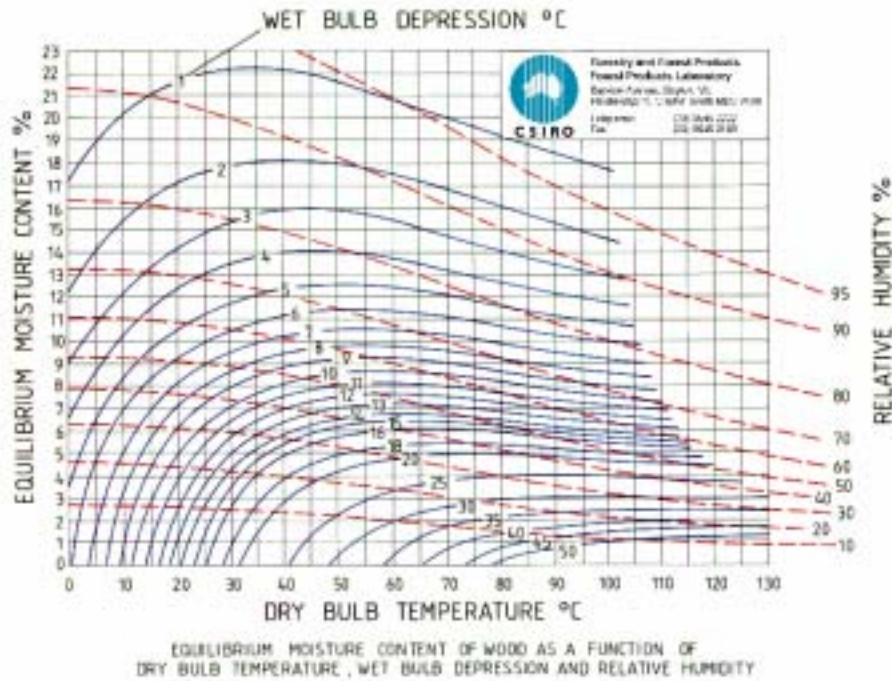


Figure 1.1 – Equilibrium Moisture Content (EMC) chart

## Wood Hygroscopicity

The term hygroscopic describes a material's tendency to absorb moisture from the air. Wood, by nature, is hygroscopic as it is able to absorb (adsorption) and expel (desorption) water to the surrounding environment depending on atmospheric conditions. The following is an account of the interactions that take place between the wood substance and water during moisture flow.

The cell wall of wood microstructure is organised as a structural system involving filamentous microfibrils, mostly cellulosic and crystalline in composition, and orientated essentially in the direction of the longitudinal axis, embedded in an amorphous matrix of noncrystalline cellulose, hemicelluloses, and lignin (Wangaard, 1979). The molecules of the amorphous regions, primarily because of  $-OH$  groups in their structure, are all capable of forming hydrogen bonds. Unlike the close-packed cellulose chains in the crystal lattice within the microfibrils, they are accessible to water molecules through diffusion from the surrounding atmosphere. Water molecules themselves are highly susceptible to hydrogen bonding. The intermolecular hydrogen bond that develops between them when a water molecule approaches within 0.3 nm (Wangaard, 1979) of the attractive site on the polymer is the basis for the hygroscopicity of wood. The adsorbed water is "bound" to molecular surfaces within the polymer matrix which expands in proportion to the quantity of water adsorbed. The microfibrillar network is distended, and the wood swells.

The range of hygroscopic activity is limited to the range of equilibria between bound water and water vapour below the fibre saturation point. Above fibre saturation, the fully swollen cell wall can take up no more water. Consequently, at this point all MC change occurs through the addition or subtraction of "free" water held in the cell cavities.



## Potential Causes and Theories Relating to moisture variation

A number of factors have been previously researched and related to the cause of moisture variation. Chafe (1991) states that factors which can affect the EMC of timber (as researched by others) include the desorption-adsorption hysteresis effect, temperature, previous drying history, stress, species and wood extractives. The following is an account of previous research regarding these factors. In addition, there are factors that do not affect the EMC but influence the drying rate of a particular board. These can cause affected boards to be at a different MC to others in a stack at the end of drying.

### 1.3.1. Moisture Sorption Hysteresis in Wood

The term hysteresis is derived from the Greek word *hysterein*, which means to “lag behind” (Skaar, 1979). The term was initially used to describe the observed lag in magnetisation of ferromagnetic material subjected to varying magnetic fields.

Hygroscopic materials such as wood also exhibit an analogous phenomenon to magnetic hysteresis, known as moisture sorption hysteresis. This refers to the lag or reduction in the sorption isotherm of EMC of wood against RH, compared with its EMC when it desorbs or loses moisture. Figures 1.2 and 1.3, respectively, show hypothetical adsorption and desorption isotherms and the approach to desorption and adsorption equilibrium with increasing time (figures extracted from Skaar, 1979).

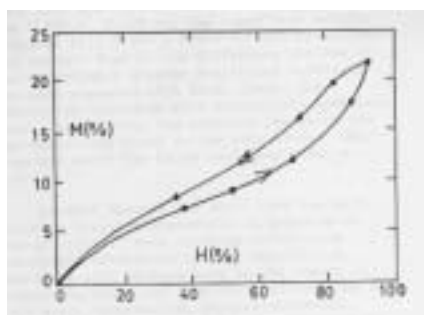


Figure A2 – Hysteresis- (Humidity)

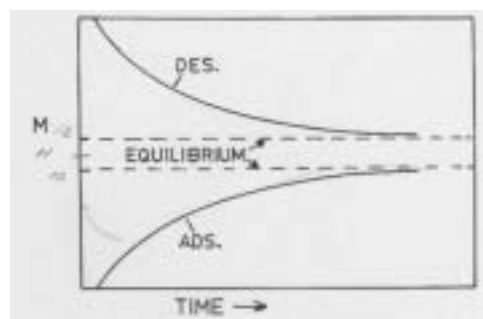


Figure A3 – Hysteresis (Time)

Kadir et al. (2001) studied the effect of different sample size and grain configuration on the EMC of red oak. Microtome slices and cross sections of increasing dimension parallel to the grain were sampled from both backsawn and quartersawn boards. The samples achieved constant weight in a steady state air environment of 43.3 °C dry bulb temperature and 84% RH. Matched batches were then created from the samples and one batch was desorbed from green while the other was adsorbed from the oven dry condition. Results showed a significant effect of sample type upon the EMC's. The greater the dimension of the cross section along the grain, the higher the desorption MC and the lower the adsorption MC. Back sawn cross sections consistently equilibrated to a higher MC for desorption than did quartersawn, while for adsorption the reverse was true. Microtome slices equilibrated to a higher MC for adsorption than for desorption. It was concluded that the overall results provide empirical evidence of stress relating to hysteresis.

Campean, Ispas et al. (1999) investigated adsorption/desorption hysteresis on a selection of timber species. The results of this study showed that the speed of desorption is much higher than for adsorption. The difference between the adsorption and desorption EMCs (hysteresis) differed between species. The highest value recorded was 10% MC ( $\pm 5\%$ ) for beech.

### 1.3.2. Theories of Sorption Hysteresis

Several theories have been proposed for explaining sorption hysteresis. The following is a summary of these theories cited in Skaar (1979).

#### 1.3.2.1. *Capillary Theories*

The earlier theories were based on the assumption that moisture sorption was primarily through capillary forces within the tiny interstices in the wood cell wall. The earliest capillary theory produced in 1911 postulated that hysteresis was caused primarily by the lower contact angle of water within these cell wall capillaries during adsorption rather than desorption. This theory was useful in explaining sorption hysteresis at high humidities but not at low humidities.

Another capillary theory was proposed in 1949 and termed the “ink bottle” theory. According to this theory, capillaries are not of even taper, but contain constrictions. During adsorption the capillaries will gradually fill from the smaller to the larger spaces. However, during desorption some of the water in the larger spaces between the narrower “bottlenecks” will tend to be trapped at lower vapour pressures, in equilibrium with those lower vapour pressures. Again this theory does not explain the sorption hysteresis occurring at lower humidities.

#### 1.3.2.2. *Sorption Site Availability Theory*

This theory of sorption hysteresis is generally thought most accurate. It is based on the reduction in the availability of hydroxyl sorption sites in wood which is absorbing moisture after having been dried. These hydroxyl groups are believed to be the primary, though not necessarily the only, sorption sites for the attachment of water molecules in the accessible regions of the cell wall.

In green wood, according to this concept, the hydroxyl groups are attached to water molecules. When the wood dries some of the hydroxyl groups are freed from the attached water molecules and mutually bond to each other as they draw closer due to shrinkage. When water is regained or adsorbed, some of the hydroxyl groups are no longer easily available to bond with water molecules. This results in less adsorption of water at a given humidity compared with the initial desorption.

As humidity increases still further, and additional water is taken up, the swelling pressures tend to break some of the hydroxyl-hydroxyl bonds, freeing some but not all of the originally water bonded hydroxyl groups or sorption sites. These are then available to be rehydrated or to absorb water molecules. During subsequent or secondary desorption the EMC is therefore higher than for absorption. However, it is generally lower than during initial desorption from the green condition, particularly at higher humidities, presumably because some of the bonds, which formed between hydroxyl groups during initial desorption, are not broken. The process repeats itself during subsequent cycling of the relative humidity, forming a more or less repetitive hysteresis loop.

#### 1.3.2.3. *Thermodynamic Hysteresis Theory*

The previous theories for describing sorption hysteresis are mechanistic as they postulate one or more specific mechanisms. The Thermodynamic Hysteresis Theory is a more general theory based on thermodynamic considerations only.

It is common knowledge that wood and other hygroscopic materials exhibit plastic or inelastic behaviour when subjected to mechanical stresses. This behaviour results in the familiar

hysteresis loop in the stress-strain diagram of wood and other completely inelastic materials. The thermodynamic hysteresis theory builds on the above concepts, where the hysteresis is explained as being caused by stress effects on the sorption isotherms of hygroscopic materials such as wood.

### 1.3.3. Extractives

Extractives are intermediate between wood substance and water in molecular weight and range widely in water solubility and volatility. In terms of their action in, or influence on sorption, extractives are difficult to classify as to being either adsorbent or adsorbate (an adsorbing substance or a substance that is adsorbed). Extractives complicate the drying, gluing and finishing of wood, however some timbers with a high extractive content are reported to be more durable and stable (Spalt, 1979). Spalt (1979) suggested that previous work uncovered extractive-related problems in the kiln drying of these woods, especially at higher kiln operating temperatures which are now coming into wider use.

#### 1.3.3.1. *Formation and Classification*

The following has been summarised from Spalt (1979).

The formation of extractives is closely associated with the transition of sapwood to heartwood. Starch and sugars stored in xylem ray and parenchyma cells are believed to be the raw materials for extractive production. At the sapwood-heartwood boundary, starch and sugars disappear and respiration rates increase. As the heartwood is approached from the sapwood, dark coloured globules that have formed and migrated to the semi-permeable cell membrane appear in the ray cells. In obligate heartwood species (those subject to the following condition) the death and disappearance of the membrane enables the extractives to migrate from the ray cells into adjoining xylem cells where they are deposited in cell lumen and infiltrate pits and cell walls. Some of these substances undergo condensation reactions that increase their molecular weight and modify their solubility and mobility.

The extractives in wood that are found in the cell wall in the greatest quantities are the polyphenols. These are primarily lignans, stilbenes, flavanoids and tannins. These substances are biosynthesised and condensed along pathways similar to lignin, and seem to have much in common with the infiltration and molecular weight building processes that lead to lignification. Deposition of the extractives into intermolecular cell wall spaces occurs when the cell wall is highly dispersed by water. Upon subsequent drying when cell wall density, strength and stability are developed, the non-volatile extractives remain as a permanent adsorbate that retains the cell wall in a partially swollen state. This phenomenon has been commonly labelled as bulking of the cell wall.

#### 1.3.3.2. *Effects of Extractives on Timber Properties*

Previous research has shown that extractives can dramatically affect the water-vapour sorption of wood.

The role of extractives in monomolecular sorption was presented by Soriano and Evans (1997). It was stated that in sorption and shrinkage studies of six Argentine woods, two species namely: *Schinopsis balansae* (Quebracho colorado santiagueno) and *Hymenaea courbaril* (Algarrobo blanco) were observed to have relatively low EMCs at 97% RH. It was found that high tannin contents displace void volume in wood, resulting in low EMCs. This indicated that in this case the extractives occupied bonding sites usually occupied by water, thus have a bulking effect.

Similarly studies have shown that the fiber saturation point of once-dried black walnut decreased from 31% in the unextracted condition to 28% after removal of hot water-soluble extractives. This led to the conclusion that the extractives in black walnut are more hygroscopic than the cell wall and that water bound by extractives is absorbed to a greater extent than water in the cell walls. Soriano and Evans (1997) state, 'In most sorption studies reported, differences in sorption

behaviour are often attributed to the bulking effect and the hygroscopicity of extractives compared to other cell wall components. Furthermore the effect of extractives has been deduced from sorption isotherms fitted using known sorption equations based on the concept of continuous layering of sorbed water on active surfaces.' Theoretical studies of selective sorption, however, point out strongly that sorption of water is selective of sorption sites, and the progression of sorption with increasing RH remains selective as well.

All previous extractive versus EMC research, as cited by Spalt (1979), indicate a reduction in the EMC values of wood samples which have had a significant percentage of extractives removed compared with unextracted control samples. Various methods of extracting extractives were used including soaking in benzene alcohol, and flushing with hot or cold water.

Spalt (1979) also cited that extractive levels were generally inversely proportional to shrinkage levels. This can be attributed to the bulking nature of the extractives.

The extractive properties themselves can change with temperature and hence change the overall wood properties. For instance, at ambient temperatures extractives act as relatively benign low-volatile adsorbates in the cell wall which displace water in larger voids. At temperatures above approximately 50°C (Spalt, 1979), the extractives in moist wood appear to become more active adsorbates that move in response to concentration gradients. In this way, they may participate in sorption and increase the overall shrinkage. As a mobile material, extractives may also serve to plasticise the cell wall, especially in desorption. The added plasticity may reduce warp related defects in kiln drying but may exacerbate collapse (Spalt, 1979).

#### 1.3.4. Species

Predictions of the expected EMC for timber are frequently made by reference to published EMC charts for relative humidity versus temperature, which often give values founded on amalgamated data for a number of species. When applying such charts to specific species, discrepancies can be substantial (Ahmet, Dai et al., 1999).

Ahmet, Dai et al. (1999) previously demonstrated that the EMC for a wide range of species, conditioned in the same environment, could vary substantially. As an example, in one investigation MCs spanned 12.8 to 21% after conditioning at 85% relative humidity, at a temperature of 20°C.

Ahmet, Dai et al. (1999) produced individual sets of EMC values for three commercially important species for interior use in the UK. The purpose of this work was to provide a powerful diagnostic tool for both specifiers and consumers in investigations of mis-supply or mismatching of MC and service conditions. As part of this experiment a pilot study was performed to investigate the following issues: 1) the effect of sample size on EMC for a given condition; 2) the influence of drying history on the final EMC; and 3) whether observable differences occur in the final EMC between samples conditioned in large commercial environmental cabinets and those conditioned in small-scale chambers containing saturated salt solutions.

The results of the pilot study indicated that systematic differences resulting from drying history (air and kiln drying) and sample size were observed. The differences in drying history were very small and not significant. The differences in EMC values in varying sample sizes was explained by the substantial differences in the ratio of surface area to sample volume. Inconsistencies between the commercial built chambers and the prototypes were negligible. The three species used in the preliminary experiments all showed consistent variations in EMC from the commonly used RH versus temperature chart over a range of RH used.

Wengert and Mitchell (1979) suggest that although the proportion of hemicellulose, holocellulose, and lignin may slightly influence the sorption behaviour between species, extractive levels cause much of the variation.

### 1.3.5. Stress

Previous research has shown that internal and external stresses can affect the MC of wood at equilibrium. Simpson (1971), by inducing either compressive or tensile forces in red oak samples proved conclusively that MC decreases when wood is compressed and increased when wood is subjected to tension. The rate of MC per unit stress was greater for specimens loaded in tension than those loaded in compression, and the effect of stress induced moisture change was more pronounced in the tangential direction than in the radial direction.

Stress effects are not necessarily confined to external stresses. Stresses can result from internal factors such as moisture gradients, which, if severe enough during drying will result in casehardened timber. Microscopic tissue anisotropy due to a) rays and differences between earlywood and latewood, b) fibril orientation differences in the S1 and S3 layers compared to the S2 layer, and c) interfibril bonds which limit swelling between fibril, also result in causing internal stresses.

### 1.3.6. Specific Gravity

Research conducted by Chafe (1991) show that a relationship also exists between wood specific gravity and EMC. An examination of wood blocks and thin sections of *Eucalyptus regnans* (mountain ash) showed that for each of three nominal EMC's (17%, 12%, 5%) actual MC was positively related to specific gravity.

### 1.3.7. Temperature

A number of researchers (as cited in Wengert and Mitchell, 1979) have reported the suppressive effect that exposure to high temperatures for lengthy periods of time has on wood EMC. Studies have been undertaken on the physical and mechanical properties of high temperature dried wood that indicate the reduction in EMC through high temperature drying is of the same magnitude. The reduction is approximately between 0.5 to 3 percent compared with conventional temperature kiln drying and between 1 to 5 percent when compared to air drying (Wengert and Mitchell, 1979). The magnitude of reduction is affected primarily by species, schedule, initial MC before equalisation and extractive content.

The most widely used explanation for the thermal reduced reduction in hyroscopicity is the hydrolysis reaction in the degradation of the hemicellulose that results in the reduction of sorption sites. Other explanations have been offered such as the MC reduction due to large drying stresses created during high temperature drying, or the hysteresis effect created in the high temperature kiln.

Kubinsky and Ifju (1974) studied the effect of steaming on wood properties of red oak. The material was converted into 24mm cubes and steamed at atmospheric pressure for various lengths of time, ranging from 1-1/2 to 96 hours. The steaming process lowered the EMC of the samples. This was attributed to a decreased bulking effect due to the reduction of extractive levels, and to a more mutual bonding of OH-groups.

### 1.3.8. Mechanical

Mechanical treatments refer to the mechanical breakdown of solid wood. As the wood is broken down, it becomes slightly more absorptive. This may be due to a mechanical breakdown of the crystallinity of the fibres (Wengert and Mitchell, 1979).

### 1.3.9. Chemical

Chemical treatments can affect wood and its sorption properties in many ways and by modifying the extractives and/or cellulose constituents.

### 1.3.10. Radiation

The effect of gamma radiation on Sitka spruce wood shows a distinct decrease in hygroscopicity (in the order of 1 to 2% with a radiation of  $10^8$  rads) (Paton and Hearmon, 1957).

## Chapter 2. Mill Study

### Introduction

An extensive study at Hurfords Building Supplies sawmill was conducted to investigate the cause of the moisture variation problem. According to the managers of Hurfords Building Supplies (NSW) Pty. Ltd., large variations in MC at equilibrium occur in regrowth spotted gum (*Corymbia maculata*) after final drying. Hurfords management believe the problem is not caused by poor practices or inadequate kiln control. They suggest that the problem is more likely to be a function of inherent properties of the resource and refer to examples of timber of the same species equilibrating to a final moisture content very different to other timbers of the same species. Minutes from discussions with Hurfords management are provided in Appendix A.

The case study at this mill was performed predominantly to examine appropriate variables of regrowth spotted gum, from the log to final dried product, in order to obtain problematic material and thus establish the cause (and extent) of the problem. The variables examined in this study were:

- Coupe location,
- board location within a log,
- MC of boards before and after pre-drying,
- MC of boards after kiln drying,
- location of board within a stack,
- Airflow and temperature distribution during kiln drying.
- Board length.
- Sawn orientation

### Trial Methodology

#### Sourcing and Tagging of Logs

Forty-five regrowth spotted gum logs were segregated in the log yard into four groups pertaining to different coupe locations. The four locations were from surrounding areas of Northern NSW, namely: two coupes side by side at Woodburn, one coupe at Banyabba, and one coupe at Tarre/Kiwarrka.

Each log was cross cut into two to three billets depending on log quality and size. Operational staff at Hurfords, performed this task, as per their standard procedures.

Three logs from each group (twelve logs) were chosen for tagging with specially designed end tags used to determine board location within a log after processing. Each billet from each log was also tagged at both ends. These tags are made of paper and are adhered to clean-cut ends of logs using Boncrete™ glue. Care must be taken to ensure that the tags do not become wet during the curing of the glue, which takes approximately two days depending on weather conditions. The tags themselves contain a printed pattern of labelled concentric circles spaced 10mm apart with labelled radial lines spaced 10° apart (see figures 2.1 and 2.2). The tags are

paired, having the same identification number but with different symbols (^ and @), so that the top end and butt end of the log/board, in relation to the tree, can be recognised. All labels and symbols are located on the template in such a way that each board sawn from the tagged logs are easily identified in terms of radial, tangential and longitudinal (in terms of top and butt) position, and specific log number. The templates were adhered to each log so that the centre of the concentric circles were placed over the pith and the 0° radial lines of the top and butt templates were orientated along the same longitudinal plane of the log.



Figure 2.1 - Log tags



Figure 2.2 - Tagged billets

The remaining logs billets were colour coded on each end using four different coloured spray paints denoting each of the four coupe locations (see figure 2.3).



Figure 2.3 - Colour tagged logs.



## Sawing, Stacking and Pre-Air Dry Analysis

Each billet was converted into predominantly back sawn boards of nominal (does not include overcut) dimension 100 × 25mm using Hurford's standard log conversion procedures for the production of flooring boards. Flooring boards were targeted in this study for the following two reasons.

1. The occurrence of complaints concerning unacceptable variations in MC of this finished product is the greatest, and
2. The final stage of this study involves using a resistance type moisture meter to measure MC on one face of all of boards utilised leaving unsightly holes. Therefore the board face that has not been tested can be dressed as the top face and still be used for flooring. The ends of the billets were not docked during conversion in order to maintain the identity of the sawn boards via either the end tags, or coloured markings.

The boards were blocked packed off the green chain and were immunised (boron) against insect attack in a pressurised treatment vessel.

The boards were then stripped into four racks with approximate dimensions of 6m x 1.8m (wide) x 1m (high). The four racks consisted of a total of 1351 boards. During stripping each board was individually weighed (see figure 2.4) to extrapolate approximate initial average MC of each board from actual MC measurements conducted after kiln drying. Two sample boards (one each side) were included within each rack to monitor MC during kiln and air-drying in order to determine the transition between air and kiln drying and the kiln drying end point. During stripping each board was individually numbered and the position of each board within the stack was noted. The racks were stacked (see figure 2.5) and placed in the air-drying yard.



Figure 2.4 - Weighing boards during racking



Figure 2.5 - Completed stack ready for air-drying

### **Air Drying**

The mill staff periodically monitored the sample board weights to determine when kiln drying should begin. In accordance with the air/kiln dry schedule, provided by Hurfords, this should occur when the average MC of the sample boards reaches approximately 15-20%. According to the Hurfords management greater variation in MC after final drying occurs when kiln drying begins at an average MC of 18-20%. Therefore, an MC value of 19% was chosen as the target air-drying end point MC, so as to exacerbate MC variation and provide an adequate number of samples for further analysis. After air-drying for approximately nine weeks, the material was deemed ready for kiln-drying based on the sample board MCs.

Before kiln drying each rack was de-stripped and approximately half of the boards were reweighed to determine MC after air-drying. Only half of the boards were weighed at this stage due to time constraints. As approximately half of the material consisted of template tagged boards and it was to be these boards that the most in-depth analysis was to be undertaken on they were targeted for weighing. The boards were re-stripped to their original positions within each rack. The racks were restacked in the same order as used during air-drying (see figure 2.5) and placed in the kiln.

### **Kiln Drying**

The kiln used was an Incomac™ conventional drying kiln. The entire charge consisted of four stacks, each stack consisting of four racks. The four stacks were orientated two deep × two wide. The kiln load consisted of the research stack plus three other air-dried stacks of similar spotted gum flooring material. Figures 2.6 and 2.7 show the kiln at various stages of loading.



Figure 2.6 - Research stack



Figure 2.7 - Full kiln charge

Prior to starting the kiln, air velocity uniformity was measured using an anemometer. The air velocity was set to 2m/s as determined by the kiln-drying schedule used by Hurfords. Over a 2-dimensional grid, the measurements were taken at various locations on one face of the research stack as air was expelled from this face. The measurements were taken at 7 evenly spaced locations in the horizontal direction and at 7 locations in the vertical direction, making a total of 49 measurements for each individual rack. Air velocity measurements were also taken between the stacks (bearer gluts).

A series of eight thermocouples were placed on one face of the stack 1.5m in from each end of each rack (see figure 2.8). This allowed real time measurements of temperature distribution vertically and horizontally at the stack face throughout the entire kiln drying process. The temperatures were measured at 15 minute intervals.



Figure 2.8 - Thermocouple

The kiln schedule used is given in table 2.1.

Table 2.1 - Kiln schedule

Time (hrs)	Temp (deg C)	RH%
2	35	60
3	40	60
5	45	60
7	50	60
9	50	57
11	55	57
17	56	53
29	60	52
41	60	49
65	65	43
105	65	35
106	63	45
107	63	58
108	63	64
110	63	68
114	65	73
132	65	70
144	55	68
150	52	65

After 105 hours, an equalisation period at an approximate EMC of 11% was performed for 45hours.

## Identification of over dry and under dry timber after kiln drying

After kiln drying and subsequent equalisation (to 11% MC) was complete, the rack was de-stripped and every board tested for average MC. During this process a calibrated resistance type moisture meter was used to determine the average MC of each board. The measurements were taken at a point in the centre of each board at a depth of approximately 1/3 the thickness, in accordance with AS/NZ 4787:2001 –Timber-assessment of drying quality. Each board was re-weighed again for the purpose of extrapolating the MC of the boards before air and kiln drying using the previous board weights measured.

Over dry or under dry boards were then selected by the deviation of the average MCs from the expected EMC of the charge (11%). Fifty boards with the highest positive MC deviation and 50 boards with the lowest deviation were segregated from the original boards. Additionally 50 boards with the lowest level of MC deviation were segregated as control boards.

Finally, the selected boards were block stacked, wrapped in impermeable plastic and transported to Queensland Forestry Research Institute – Salisbury Research Centre, Queensland for further testing.

## Testing of selected material

Each board selected was tested for average MC at varying positions along the length using the oven dry testing method, in accordance with AS/NZS 1080.1 – Methods of test – Timber-Moisture content. A 400mm length section was cut from the end of each board and discarded to negate the effects of end drying. Each board was then cut into 550mm length sections, a 25mm length sections was then cut from each end to calculate average MC using the oven dry method. The MC of each 500mm length section was calculated as the average MC of the two 25mm section cut from each end. Each 500mm length section was appropriately labelled with the original board number consecutively appended with a,b,c etc. As the original board length varied (dependent on the original billet size) differing numbers of 500mm length sections were produced from each board.

Additional board attributes were measured during board dissection, namely; original board length, sawing orientation (back sawn, quarter sawn or transitional) and centre reference point at top and butt ends of boards (originating from templated billets).

Each of the 500mm length sections were end coated with sealant and re-wrapped in impermeable plastic for further testing. However, due to the nature of the MC results obtained from the 25mm sections, further testing was terminated.



## Results

### 2.3.1 Sawing, Stacking & Air Drying

Approximately the same volume of logs was sawn from each of the four coupe locations for the trial. Table 2.2 shows the percentage of boards from each location used in this trial. Both, the ratio of the total number of boards and the ratio of tagged boards (converted from tagged logs) are given.

Table 2.2

Coupe	Total Boards		Tagged Boards	
	# Boards	% Total	# Boards	% Total
Woodburn1	154	12	117	23
Woodburn2	550	41	141	28
Banyabba	296	22	121	24
Tarre	332	25	124	25
Total	1332		503	

The data shows that relatively even proportions of tagged boards were included in this study, even though 41% of all of the boards used were from the Woodburn1 coupe and only 12% came from the Woodburn2 coupe. This was because the volume of timber converted from each coupe exceeded the amount required for the actual trial. When the material was racked, the most convenient material was removed from the block packs first and so material from the Woodburn1 coupe was predominantly left over. An exception to this rule was the tagged boards, which were all used, hence the even coupe proportions.

The air drying phase of this trial took approximately 68 days. The initial and final average MC of the sample boards were 47.6% and 19.1%, respectively. The air drying period was slower than expected due to a two week period of constant rain.

The kiln drying process took approximately 6.25 days including equalisation.

### 2.3.2 Kiln Conditions

#### 1.3.2.4. Air Velocity

The air velocity was set to 2m/s using the PC kiln control unit. Measurements were taken over a two-dimensional grid at various locations on one face of the research stack as air was expelled from this face.

The measurement results are given in appendix B, section B.2.1, where rack numbers are sequential, i.e. rack1 denotes the top rack (nearest the roof of the kiln), and rack 4 denotes the bottom rack. Table 2.3 contains the average air velocity values for each stack, the total average, maximum and minimum values recorded. Figures 2.9 - 2.12 graphically illustrate the air velocity measurements as a two-dimensional grid.

Table 2.3 - Air velocity results

	Average Air flow Values		
	Average	Minimum	Maximum
Rack1	1.8	1.3	2.3
Rack2	1.8	1.0	2.4
Rack3	1.9	1.5	2.6
Rack4	1.9	1.3	2.3
Total	1.8		

The average air velocity results for each rack are comparatively consistent with an average value of 1.8m/s over the entire rack face (excluding gluts). This is 10% below the set value of 2m/s but is very accurate for a kiln of this size.

The minimum and maximum values recorded seem to indicate quite large variations, however the air velocity maps (figures 2.9-2.12) show that the lower values recorded occur predominantly at the rack edges where baffling is rarely perfect. Overall the airflow results show good uniformity for each rack in both the horizontal and vertical directions.

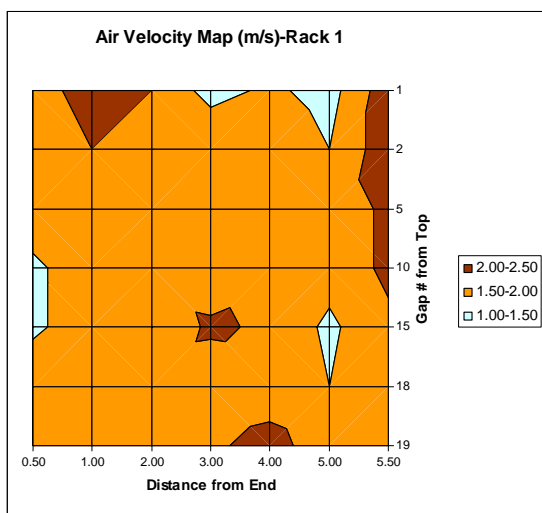


Figure 2.9 - Air Velocity Map Rack 1

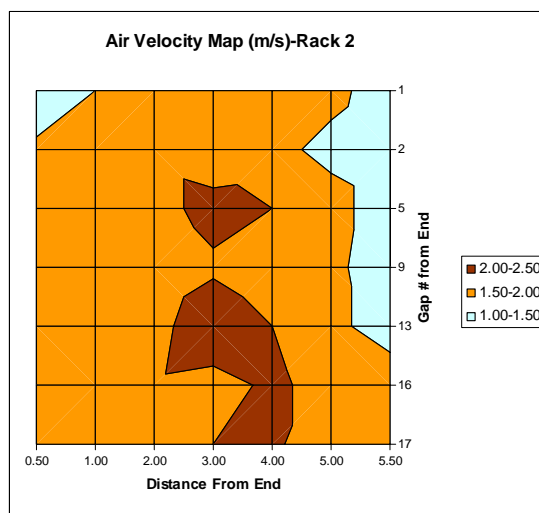


Figure 2.10 - Air Velocity Map Rack 2

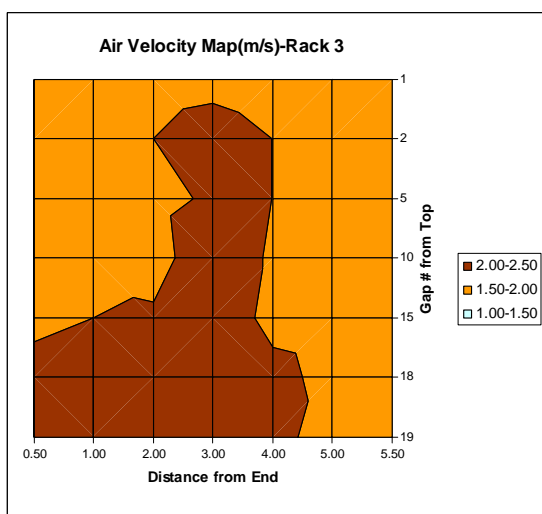


Figure 2.11 - Air Velocity Map Rack 3

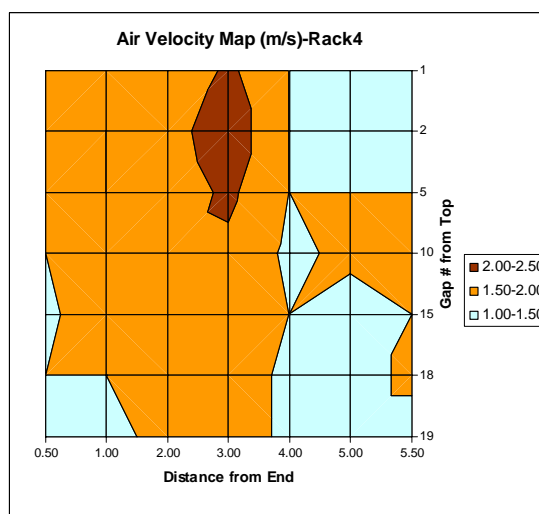


Figure 2.12 - Air Velocity Map Rack 4

1.3.2.5. *Temperature*

Figure 2.13 is a temperature versus time graph of these real time thermocouple temperatures. Appendix B.2.2 contains the thermocouple data used to produce this graph.

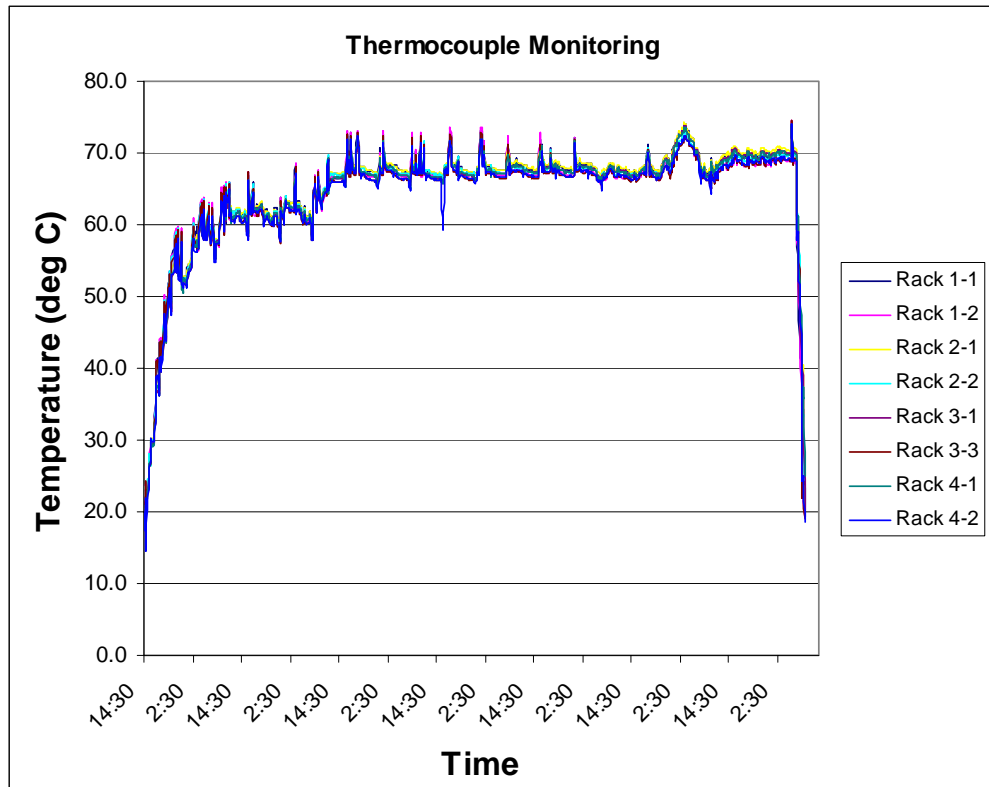


Figure 2.13 – Thermocouple temperature graph

The resulting graph indicates that the temperature variation through the research stack was consistent both vertically and horizontally. The maximum difference recorded between thermocouples was approximately 3°C. This is insignificant for a kiln of this size. The spikes shown on the graph represent either fan reversals or kiln openings during periodic measurement of sample board weights.



### 2.3.3 Moisture Content (Moisture Meter)

Using a calibrated resistance type moisture meter, the corrected (for temperature and species) MC of each board used in this study was measured. From these values, estimated initial and air-dry MCs of the boards were calculated. These values were calculated to observe if a correlation existed between, oven drv MCs calculated for the problematic selected material, and the estimated MCs of the same material before and after air-drying.

The estimated MCs of the boards were calculated using the following formulae 2.1 and 2.2.

Firstly the estimated oven dry weight of each board was calculated using,

$$W_{ode} = \frac{W_{kd} \times 100}{MC_m + 100} \quad (2.1)$$

where  $W_{ode}$  = Estimated oven dry weight.

$W_{kd}$  = Kiln dried final measured weight.

$MC_m$  = Kiln dried moisture meter measured MC.

The initial and air dried estimated MC of the boards were calculated using,

$$MC_{i/a} = \left( \frac{W_{i/a} - W_{ode}}{W_{ode}} \right) \times 100 \quad (2.2)$$

where  $MC_{i/a}$  = Either initial of air dried moisture content.

$W_{i/a}$  = Either initial or air dried measured weight.

The estimated initial and air dried MCs, kiln dried moisture meter MCs, associated weights and corresponding coupe numbers for each board are given in appendix B.1. The coupe numbers 1 to 4 correspond to Woodburn1, Woodburn2, Banyabba, and Tarre/Kiwarra coupes respectively. The average, minimum and maximum MCs were calculated from the initial air dried and final dried estimated MC data and is tabulated below (table 2.4).

Table 2.4 – Inital, air dried and final dried MC analysis

	Moisture Content (Whole Boards)		
	Initial	Pre-Kiln Post-Air	Final
Average	52.4	21.5	11.2
Maximum	85.8	28.7	16.0
Minimum	28.5	17.4	8.0

The maximum and minimum MC variation is reduced dramatically from the initial value of 57.2% to the air-dried (pre-kiln post-air) value of 11.3%. A further reduction is evident after final drying (8%).

The average final dried MC (11.2%) is close to the target MC (11%).

The maximum and minimum variation after drying was not as large as was desired in terms of the objective of this study. Only five boards (0.4% of total) had a measured MC below 9% and 3 boards above 15% MC (0.2% of total). In fact 96% of the boards had moisture contents in the range of 9 to 13%MC ( $\pm 2\%$  of target MC).

A greater maximum/minimum MC variation was expected after kiln drying. Hurford's staff has previously measured greater variations (boards with MCs over 18% have been recorded).

### 3 Selected Material Testing (Oven Dry MC)

As detailed in section 2.2.5, 150 boards were selected for further testing. These boards consisted of the 50 wettest, 50 driest and 50 boards with a measured MC closest to the target MC (11%).

Each board was cut into 500mm sections such that a 25mm section was cut from each end for oven dry MC testing. The results of these tests are given in appendix B.3.1. The average MC of each 500mm section was calculated as the average of the two 25mm sections cut from each end. The average MC of each whole board was calculated as the average of the 500mm sections cut from that board. Table 2.5 summarises these results tabulating the average, maximum and minimum values for the whole volume of 25mm, 500mm and full length boards respectively.

Table 2.5 – Summary of oven dry test results

	Moisture Content Data		
	25mm Sections	500mm Sections	Whole Board
Average	10.6	10.6	10.6
Maximum	13.5	13.4	12.8
Minimum	7.9	8.5	9.2

The summary of results further emphasises the lack of problematic MC variable material obtained from this study. From the 150 boards selected 822 25mm sections were oven dry tested for MC. The range from this large selection of samples was minimal (7.9% to 13.5%). The maximum and minimum MCs for the whole boards ranged from 9.2 to 12.8%.

A low  $r^2$  correlation of 0.41 was calculated between the average board oven dry MCs and the measured moisture meter MCs. This is illustrated in figure 2.1.4.

Additional board attributes were also measured during board dissection, namely; original board length, sawing orientation (back sawn, quarter sawn or transitional) and centre reference point at top and butt ends of boards originating from templated billets. These attributes were measured as potential variables to analyse their correlation against the existence of problematic material. However, as no problematic material was observed these attributes were not analysed. The data has been included in this report (see appendix B.3.2.).

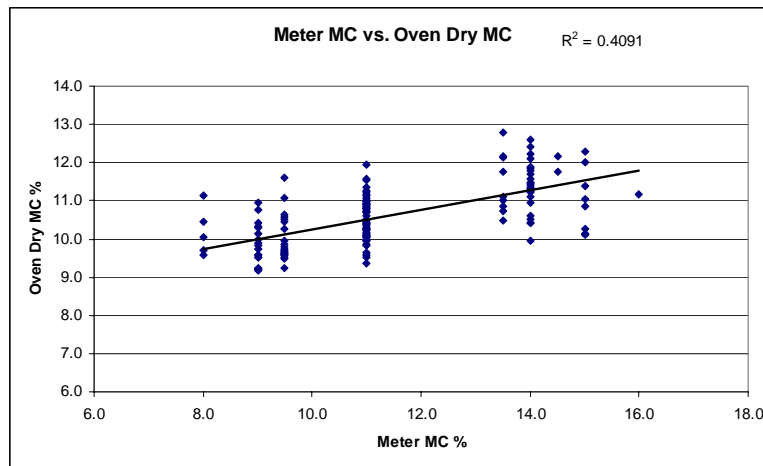


Figure 2.14 – Moisture meter MC vs. Oven dry MC

## Conclusions

The main outcome from this study was the unexpected lack of material with undesirable final dry moisture contents. This was unexpected due to previous history at the site when drying this material using similar drying techniques. Exacerbation of problematic material through initialising kiln drying at higher than normal moisture contents did not occur. Given this and the large volume of material tested, from a production point of view, the results are exceptional.

An additional outcome from the mill study was the greater variation in MC readings obtained from the moisture meter compared with oven dry results. This is also emphasised by the low correlation observed between the two. It is common knowledge in the industry that moisture meters are not as accurate as the oven dry method for determining MC.

It should be noted that the kiln conditions, in terms of temperature and air-flow distribution, were also exceptionally stable with little variation. With this in mind and the lack of problematic material obtained, it can be theorised that the initial assumption that unacceptable variation in final moisture contents is caused by variations in timber properties may only be partly true. Kiln performance and drying practice may also be factors causing the reported problem.

Although this section of work was prevented by the lack of obvious problematic material it is believed that by broadening the scope of this project could be continued in the future. The final section of this report (section 3.5) proposes recommendations toward furthering this study based on the results obtained throughout this report.

## Chapter 3. Dry Stock Appraisals

### Introduction

The dry stock appraisals were undertaken to determine the extent of moisture content variation through the inspection of randomly selected dried stock. The appraisals were conducted at various commercial hardwood sawmills which were collaborating in this project. The inspections were conducted at Clennett Timber (Tas), Hume and Kerrison Pty. Ltd. (Tas), Hurfords Building Supplies Pty. Ltd. (NSW), J. Notaras & Sons Pty. Ltd. (NSW), Hyne & Son Pty. Ltd. (QLD). At each mill, the two species that are processed to produce the highest volume of quality joinery or flooring sawn timber were appraised. As such, the species investigated were *Eucalyptus delegatensis*, *E. regnans*, *Corymbia maculata*, and *E. pilularis*.

It should be noted that due to the sensitive 'commercial in confidence' nature of the outcomes, the results are not linked to the commercial names of each sawmill. Rather, each sawmill is given a number from one to five (that does not correspond to the order given above). Additionally, species names are not given for each mill due to obvious geographical linkages.

The appraisals themselves involved measurement of MC average and gradient from a material subset. These two properties are the most relevant for investigating MC variation. The average MC is directly related to the desired target MC sought after drying. Additionally, the moisture gradient (difference in MC across a set distance of the case and core of a board) is important as it is linked to the MC variation through the thickness of a board.

### Methodology

Dried stock appraisals were conducted in accordance with AS/NZS 4787:2001 – Timber – Assessment of drying quality.

Using this standard as a guide, assessment of average MC and MC gradient were investigated on dried stock to give drying quality class classifications for these two properties. It should be noted that to easily explain the procedures used, the following methodology section contains excerpts from the aforementioned standard.

### Initial Information

In order to compare the quality of grade output the following information was obtained from the management of each participating site:

- What are the most common two species of dried quality stock with a cross sectional thickness not greater than 80mm (maximum thickness at which standard is valid) produced?
- What are the cross sectional dimensions of these products?
- What is your target final average MC for these products?

At each mill, after the initial questions were answered, sampling was undertaken on 25mm and 50mm thick rough sawn material, and 19mm thick dressed material of the target species, dependant on availability of stock.

## Sampling

At each mill, forty boards of each species were tested for average MC and MC gradient. The boards were selected randomly from either dressed or rough sawn packed stock, so that five individual pieces were selected from each of eight packs. Where this was not possible, material was selected directly from the dry chain such that eight groups of five boards were selected leaving sufficient time between each group of boards to cover an approximate volume of one pack. The number of samples chosen was sufficient to cover all quality class groups (see section 3.2.4), as specified by AS/NZS 4787:2001.

## Measurements

All measurements were taken at least 400mm from the end of a test piece. Additionally, the ambient air temperature where the packs were stored was measured before testing. The following summarises moisture content measuring procedures.

- **Average Moisture Content**

The average MC was measured using an insulated electrode resistance type moisture meter (pre calibrated to Douglas Fir) at a depth of  $\frac{1}{3}$  of the thickness of each test piece (denoted by  $MC_{1/3}$ ).

- **Moisture Content Gradient**

Assessment of MC gradient was carried out by successive MC measurements, on the same cross-section of each sample piece at two defined depths. The first reading was taken at a depth of  $\frac{1}{6}$  the thickness or 5mm, whichever was the larger (denoted by  $MC_{1/6}$ ). The second reading was taken at a depth of  $\frac{1}{2}$  the thickness of the test piece (denoted by  $MC_{1/2}$ ).

All MC measurements were corrected for temperature and species in accordance with AS/NZS 1080.1 – Timber Methods of Test – Moisture Content.

## Quality Class Specifications

In accordance with AS/NZS 4787:2001 drying quality class specifications can be made dependant on the results of the MC gradient and average MC measurements.

For average MC, 90% of samples must comply with moisture content tolerances from the target average MC (denoted by  $MC_t$ ) as specified by the sawmill management.

Table 3.1 lists the allowable range and associated quality class for 90% of all MC readings around the target MC.

Table 3.1 – Moisture content quality class specifications

Quality class	Allowable deviation between measured moisture content ( $MC_{1/3}\%$ ) and target moisture content ( $MC_t\%$ )				
	$MC_t = 8$	$MC_t = 10$	$MC_t = 12$	$MC_t = 14$	$MC_t = 18$
Class A	1	1	2	3	3
Class B	1	2	3	4	5
Class C	2	3	4	5	5
Class D	3	4	5	6	7
Class E	4	5	6	7	9

For MC gradients, 90% of samples must adhere to MC tolerances from case ( $MC_{1/6}$ ) to core ( $MC_{1/2}$ ).

Table 3.2 lists the maximum allowable deviation in MC between  $MC_{1/2}$  and  $MC_{1/6}$ , by target MC and quality class.

Table 3.2 – Moisture gradient quality class specifications

Quality class	Allowable deviation between core ( $MC_{1/2}$ ) and case ( $MC_{1/6}$ ) moisture content by target moisture content ( $MC_t\%$ )				
	$MC_t = 8$	$MC_t = 10$	$MC_t = 12$	$MC_t = 14$	$MC_t = 18$
Class A	1	1	2	3	3
Class B	1	2	3	4	5
Class C	2	3	4	5	5
Class D	3	4	5	6	7
Class E	4	5	6	7	9

The quality class descriptions described in AS/NZS 4787:2001 are as follows:

Class A – caters for specific end uses and very specific requirements for drying quality;

Class B – applies where tight control over drying is required to limit 'in service' movement resulting from changes in equilibrium moisture content;

Class C – applies where higher drying quality is required and the final use environment is clearly defined;

Class D – applies when the final use environment is more clearly defined but again the drying quality requirements are not considered high; and

Class E – applies when the final use and drying quality requirements are not high.

## Results

All measurements were conducted in accordance with the methodology (section 3.2). Table 3.3 summarises the dried stock quality assessment results for each sawmill. Contained in the table are the, species identification number (for some mills only one species was available for testing), thicknesses for each species, target moisture content, average MC grade quality class, and the MC gradient grade quality class (see 3.2 for description of class classifications). Full sets of results are included in appendix C.

Table 3.3 - Dried stock quality assessment results

Species	Site 1		Site 2		Site 3		Site 4		Site 5
	1	2	1	1	1	2	1	2	1
Thickness	19mm	19mm	25mm	50mm	19mm	19mm	19mm	19mm	25mm
Target MC (%)	12	10	12	12	10	10	10	10	12
Average MC Grade	B	A	C	Fail	B	B	B	B	A
MC Gradient Grade	A	A	B	C	B	B	A	A	D

In terms of the objective, the following results from each site are considered to be of importance:

**Site 1:** The resulting grade quality of the selected samples for this site (species 1 and 2) are high quality in terms of average MC and MC gradient. However sample number 7, species 1 (see C.1.1), had a moisture content value considered to be much higher or wetter than the other samples, which is a cause for concern. This sample would be viewed as being a problematic piece in terms of the scope of this project.

**Site 2:** For the 25mm material the average MC quality was poor (see C.2.1). This is because the majority of the board average MC values were higher than the target MC of 12%. This indicates insufficient drying to reach the target MC. Additionally, samples number 2, 11 and 18 (see C.2.1) have considerably higher average MC values than the other samples. Again these samples would be viewed as being problematic pieces.

The grade quality results for the 50mm material were very poor (see C.2.2). The average MC value for each board was well above the target MC of 12%, with 47.5% of boards failing to even receive a quality classification (greater than 6%MC above target). The average MC of all samples was 18.1%. This material had definitely not been dried for a long enough period to reach the desired target MC. Due to insufficient drying it is not possible to identify problematic moisture variable timber at this stage.

**Site 3:** In terms of average MC grade, there were no over or under dry boards measured (species 1 and 2). The grade quality in terms of average MC and MC gradient was high.

**Site 4:** In terms of average MC grade, there were no over or under dry boards measured (species 1 and 2). The grade quality in terms of average MC and MC gradient was high.

**Site 5:** In terms of average MC grade, there were no over or under dry boards measured. However, the MC gradient grade for the majority of these boards (see C.5.1) were average. A result such as this is a common indicator of material that has not been sufficiently equalised to EMC conditions after drying.

**Note:** In terms of MC gradient grade quality, sites 1, 3, and 4 performed better than sites 2 and 5. This may be affected by the thinner (19mm) dressed material tested at these sites. As MC gradients generally occur such that the surface of a board is drier than the core, obviously the MC gradient will be reduced when the surfaces of a board is dressed.

## Conclusions

Through appraisals of randomly selected dried stock the extent of moisture content variation was examined at various commercial hardwood sawmills.

Although the series of appraisals were only taken on one day of production, from a random selection of material on a small cross-section of the Australian hardwood industry, the study has uncovered enough information to a) indicate that a problem does exist and b) a number of underlying issues are also in evidence. These underlying issues are predominantly concerned with drying practice. This second issue is relatively sensitive, and although a series of postulations leading to recommendations are included in these conclusions, this was not within the scope of this project and hence becomes an opportunity for further research (see section 3.5).

Analysis of data taken at sites 1 and 2 indicate the existence of small numbers of boards with average MCs much greater than other boards dried under the same conditions. The reasons for this are still yet unknown. The existence of this type of material is of great concern to the industry due to its potential to create problems between timber processors and their clients (and in application).

From the results given for sites 2 and 5 it is evident that the moisture variation/drying issue can easily be confused with issues pertaining to practice. The 50 mm material tested at site 2 specifically shows insufficient drying to the target MC. Reasons for this may be caused by; relying on MC resistance probes instead of using sample boards, incorrect use and/or using uncorrected moisture content readings of moisture meters, relying on time based drying schedules, kiln limitations, and storing material in wet climatic conditions after drying. Without further study however, only postulations can be considered at this stage.

The MC gradient quality of the material tested at site 5 was considered to be poor. The average MC quality for the same material however, was high. This seems to indicate insufficient equalisation at the end of the drying process. This is again a drying practice issue rather than an issue pertaining to timber properties.

Even though the results from the previous chapter did not produce the required results to continue this study, the results from the sawmill dry stock appraisals definitely indicate that the moisture variation problem, consisting of rogue wet material, does exist. Additionally, further questions have been raised relating drying best practice to this issue. The potential to identify the cause of this problem exists and further research is required, building on the scope of this project. Outlines containing further recommendations for continuing this study are given in the following section.



## Recommendations for Future Work

At the time of writing this report the moisture variation issue still remains unresolved. This is due to unforeseen circumstances governing the outcomes of the mill study (as detailed in Chapter Two). Results obtained in this chapter however, have given enough insight into the problem to continue this line of research in order to find a solution.

The dry stock appraisal survey has shown that the existence of the moisture variation problem may not be entirely caused by timber properties as first postulated. Rather, drying practice may also be a causal factor.

An outline of a future project to complete the research started in this project may be as follows:

- 1) Survey a greater number of sawmills throughout Australia to identify those that are experiencing problems with moisture content variation after final drying.
- 2) Perform on site investigations at sites that are experiencing the problem. This would involve personal interviews with site managers and staff. Additionally data measurement of air drying and kiln drying conditions including air velocity, humidity and temperature variation would also be conducted.
- 3) Obtain problematic material from these sites along with non-problematic control material, over a set time period, to compare timber properties. Timber property measurement could include, vessel frequency, lumen diameter, cell wall thickness, percentage of hemi-cellulose, extractive content (using both methanol + hot water extraction methods).
- 4) Perform stability measurements in a constant environment chamber on the material obtained from 2).
- 5) Provide economically feasible solutions to address the problem.

It is believed that this type of approach would not only guarantee that problematic material will be obtained for testing, but also the underlying best practice issue would be investigated.

## References

- Ahmet, K., G. Dai, et al. (1999). "Experimental procedures for determining the equilibrium moisture content of twenty timber species." Forest Products Journal **49**(1): 88-93.
- Campean, M., M. Ispas, et al. (1999). Experimental Study Concerning the Hysteresis of Sorption and Desorption for Different Wood Species. 6th International IUFRO Wood Drying Conference, Stellenbosch, South Africa.
- Chafe, S. C. (1991). "A relationship between equilibrium moisture content and specific gravity in wood." Journal of the Institute of Wood Science **12**(3): 119-122.
- Kadir, K., R. Erickson, et al. (2001). The Effect of Sample Size and Configuration on Red Oak Hysteresis. 7th International IUFRO Wood Drying Conference, Tsukuba, Japan.
- Kubinsky, E. and G. Ifju (1974). "Influence of steaming on the properties of Red Oak. Part II. Changes in shrinkage and related properties." Wood Science **7**(2): 103-110.
- McNaught, A. (1987). Equilibrium moisture content of timber. QFRI Timber Note. **23**.
- Paton, I. M. and R. F. S. Hearmon (1957). "Effect of exposure to gamma rays on the hygroscopicity of Sitka sprucewood." Nature **180**: 651.
- Simpson, W. T. (1971). "Moisture changes induced in red oak by transverse stress." Wood and Fiber **3**(1): 13-21.
- Skaar, C. (1979). Moisture Sorption Hysteresis of Wood. Rosen, H. N.; Simpson, W.; Wengert, E. M.; (Chairmen): Symposium on wood moisture content temperature and humidity relationships, Virginia Polytechnic Institute and State University, Blacksburg, Virginia, Oct. 29, 1979. 1979, 4 11; 31 ref., Forest Products Laboratory, USDA Forest Service.; Madison, Wisconsin; USA.
- Soriano, F. P. and P. D. Evans (1997). "The role of extractives in monomolecular sorption and cluster formation in thin King William pine (*Athrotaxis selaginoides* D. Don.) wood strips." FPRDI Journal **23**(1): 47-66.
- Spalt, H. A. (1979). Water-Vapour Sorption by Woods of High Extractive Content. Rosen, H. N.; Simpson, W.; Wengert, E. M.; (Chairmen): Symposium on wood moisture content temperature and humidity relationships, Virginia Polytechnic Institute and State University, Blacksburg, Virginia, Oct. 29, 1979. 1979, 4 11; 31 ref., Forest Products Laboratory, USDA Forest Service.; Madison, Wisconsin; USA.
- Wangaard, F. F. (1979). The Hygroscopic Nature of Wood. Rosen, H. N.; Simpson, W.; Wengert, E. M.; (Chairmen): Symposium on wood moisture content temperature and humidity relationships, Virginia Polytechnic Institute and State University, Blacksburg, Virginia, Oct. 29, 1979. 1979, 4 11; 31 ref., Forest Products Laboratory, USDA Forest Service.; Madison, Wisconsin; USA.
- Wengert, E. M. and P. M. Mitchell (1979). Psychrometric relationships and equilibrium moisture content of wood at temperatures below 212 deg F (100 deg C) [a review]. Rosen, H. N.; Simpson, W.; Wengert, E. M.; (Chairmen): Symposium on wood moisture content temperature and humidity relationships, Virginia Polytechnic Institute and State University, Blacksburg, Virginia, Oct. 29, 1979. 1979, 4 11; 31 ref., Forest Products Laboratory, USDA Forest Service.; Madison, Wisconsin; USA.
- Waterson, G 1997. Australian Timber Seasoning Manual. Australasian Furnishing Research and Development Institute Limited.

## Appendices

- Appendix A. Survey Meeting Minutes at Hurfurds
- Appendix B. Mill Study Data
- Appendix C. Dry Stock Appraisal Data



## Appendix A. Survey Meeting Minutes-Hurfords

Bob Engwirda is the manager of the dry mill at Hurford Hardwood – Lismore NSW. This is the site for the case study examination. The following is an account of an informal meeting held on 13/12/01.

In the past Bob has experienced problems with moisture variation particularly “wet wood” after kiln drying, predominantly with spotted gum and blackbutt.

The material is generally air dried first to below FSP and enters the kiln for final drying when the average moisture content of the material is between approximately 15% and 20%. Under his current schedule Bob states, ‘at 15%MC the material usually takes approximately 5-6 days to dry and at 18-20%MC the material takes approximately 6-7 days to dry.

Bob has trialed higher temperatures during final drying to speed up the process. The drying times were faster, however the moisture variation problem was exacerbated. A greater proportion of under-drys were present. Less variation is currently present with the slower/colder drying schedules being used. Other observations conducted by Bob were:

- a) moisture content variation seems to be worse for timber entering the kiln drying phase at higher average moisture contents (ie. 20% c/f. 15%),
- b) by observation, a large proportion of wet wood boards are quarter/transitional sawn and/or exhibit comparatively closely packed (denser) growth rings,
- c) the best method to reduce moisture variation is to over dry the material from the desired target MC to 8-9%, then steam to approximately to 13-14% before redrying at the same final conditions to 10%. Additionally, it was observed that the steaming treatment did not seem to effect the permeability (drying rate) of the material.

When sawing, Hurfords usually saw the same species for approximately 1 weeks to produce approximately 50-60 stacks of green boards. Air drying takes approximately 12 weeks and the kiln charge consists of 16 stacks. The stacks are orientated inside the kiln 4 high × 2 wide × 2 long

Graeme Palmer, was also present at this meeting, and suggested that drying at higher temperatures increases the transport rate of water movement exponentially with temperature so that the material that is more permeable will dry faster compared with the material of lower permeability. Hence a greater number of wet wood boards will be present at the end of drying.

Graeme also suggested a number of potential areas of research regarding this project as follows:

- 1) The variation trends of MC between boards has not yet been investigated when comparing the same boards at the end of air drying with those at the end of kiln drying.
- 2) Intermittent cyclic/humidity treatments during final drying.
- 3) Holding the material at a fixed EMC for a period of time towards the end of drying to equalise before drying is completed.
- 4) Drying schedule/Energy cost issue. Ie. would it be more cost effective to kiln dry at lower initial temperatures and a higher wet bulb depression initially when compared with current schedules?

















1325	10.06	46.9	8.32	21.49	7.67	12	6.85	2
1326	9.46	47.4	7.76	20.88	7.19	12	6.42	2
1327	10.15	56.4	7.99	23.09	7.27	12	6.49	4
1328	15.63	53.4	12.28	20.50	11.21	10	10.19	3
1329	17.10	44.7	14.28	20.83	13.00	10	11.82	3
1330	11.50	49.7	9.11	18.59	8.45	10	7.68	3
1331	20.81	53.5	16.74	23.51	15.18	12	13.55	2
1332	17.92	50.9	14.60	22.95	13.30	12	11.88	4
1333	20.99	60.3	16.71	27.64	14.99	14.5	13.09	4
1334	18.72	44.5	15.34	18.41	14.25	10	12.95	2
1335	18.57	42.0	15.49	18.42	14.52	11	13.08	2
1336	17.13	46.2	14.53	23.99	13.24	13	11.72	2
1337	17.49	45.8	14.36	19.67	13.20	10	12.00	4
1338	20.91	48.5	17.28	22.72	15.77	12	14.08	2
1339	22.77	47.8	18.67	21.15	17.26	12	15.41	2
1340	17.01	43.9	14.13	19.56	13.00	10	11.82	2
1341	19.63	45.3	16.04	18.70	15.54	15	13.51	4
1342	22.09	40.8	18.69	19.11	17.26	10	15.69	2
1343	17.68	46.2	14.80	22.42	13.54	12	12.09	2
1344	18.56	44.2	15.75	22.33	14.42	12	12.88	2
1345	17.93	47.6	14.98	23.29	13.73	13	12.15	2
1346	17.34	49.0	14.24	22.40	13.03	12	11.63	2
1347	18.59	51.9	15.23	24.46	13.95	14	12.24	4
1348	17.11	48.1	14.38	24.47	13.17	14	11.55	4
1349	12.45	56.5	9.71	22.06	8.83	11	7.95	3
1350	14.28	49.7	11.75	23.17	10.78	13	9.54	2
1351	11.70	44.3	9.65	19.02	9.00	11	8.11	2

A.2. Kiln Data

B.2.1. Air Flow

		Distance From End (m)						
Gap #	0.50	1.00	2.00	3.00	4.00	5.00	5.50	
1	1.8	2.2	2.0	1.3	1.6	1.3	2.3	
2	1.5	2.0	1.5	2.0	1.9	1.5	2.3	
5	1.8	1.5	1.8	1.8	1.9	1.7	2.1	
10	1.4	1.8	1.7	1.6	1.8	1.7	2.1	<b>Rack 1</b>
15	1.4	1.8	1.5	2.1	1.9	1.4	1.9	
18	1.9	1.6	1.7	1.6	1.7	1.5	1.8	
19	1.9	1.9	2.0	1.9	2.2	1.7	1.7	
	1.9	2.0	3.2	3.1	3.5	2.0	2.3	<b>Glut 1</b>
Gap #								
1	1.1	1.5	2.0	1.6	1.6	1.7	1.1	
2	1.6	1.7	1.8	1.6	1.7	1.3	1.6	
5	1.6	1.9	1.8	2.2	2.0	1.8	1.0	
9	1.6	1.8	1.6	1.9	1.6	1.7	1.0	<b>Rack 2</b>
13	1.6	1.8	1.8	2.4	2.0	1.7	1.1	
16	1.5	2.0	1.9	1.8	2.1	1.8	2.0	
17	1.8	2.0	1.8	2.0	2.1	1.6	1.7	
	3.2	3.4	3.4	3.4	3.4	3.0	2.5	<b>Glut 2</b>
Gap #								
1	1.5	1.6	1.7	1.8	2.6	1.5	1.7	
2	1.8	1.8	2.0	2.3	2.0	1.7	1.8	
5	1.9	1.8	1.8	2.1	2.0	1.8	1.8	
10	2.0	1.8	1.7	2.5	1.9	1.7	1.8	<b>Rack 3</b>
15	1.8	2.0	2.1	2.5	1.8	1.7	1.7	
18	2.3	2.0	2.4	2.4	2.2	1.8	1.6	
19	2.2	2.0	2.2	2.4	2.3	1.6	1.7	
	3.7	3.8	3.5	3.9	3.3	3.3	2.3	<b>Glut 3</b>
Gap #								
1	1.6	1.7	1.5	2.1	1.5	1.5	1.3	
2	1.6	1.5	1.8	2.3	1.5	1.3	1.5	
5	1.8	1.5	1.7	2.1	1.5	1.5	1.5	
10	1.5	1.7	1.8	1.9	1.4	1.6	1.6	<b>Rack 4</b>
15	1.4	1.8	1.6	2.0	1.5	1.3	1.5	
18	1.5	1.5	1.7	2.0	1.3	1.3	1.6	
19	1.4	1.4	1.6	2.0	1.3	1.3	1.3	
	3.0	3.4	3.7	3.2	2.7	2.8	2.5	<b>Glut 4</b>

B.2.2. Temperature

Table with 11 columns: Date, Time, Rack 1-1, Rack 1-2, Rack 2-1, Rack 2-2, Rack 3-1, Rack 3-3, Rack 4-1, Rack 4-2. Rows include dates from 29/5 to 31/5 and times from 14:30 to 20:15.

Table with 11 columns: Date, Time, Rack 1-1, Rack 1-2, Rack 2-1, Rack 2-2, Rack 3-1, Rack 3-3, Rack 4-1, Rack 4-2. Rows include dates from 30/5 to 1/6 and times from 8:00 to 14:30.







4/6	15:45	70.3	68.7	70.9	69.5	70.2	68.5	70.0	68.5
4/6	16:00	70.6	69.2	70.9	69.9	70.6	69.5	70.5	69.7
4/6	16:15	70.3	68.9	70.5	69.3	70.1	68.7	69.5	69.0
4/6	16:30	69.4	68.4	70.1	69.4	69.7	68.7	69.5	68.8
4/6	16:45	70.1	69.0	70.5	69.6	69.8	69.0	69.8	68.8
4/6	17:00	69.8	68.8	70.4	69.8	70.0	69.0	69.8	68.9
4/6	17:15	69.5	68.5	70.1	69.3	69.8	68.5	69.7	69.1
4/6	17:30	69.8	68.6	69.8	69.3	69.5	68.4	69.2	68.4
4/6	17:45	69.8	68.7	70.0	69.3	69.6	68.5	69.2	68.4
4/6	18:00	69.7	68.3	69.9	69.3	69.3	68.3	69.5	68.6
4/6	18:15	69.1	68.0	69.8	68.8	69.4	68.3	69.5	68.6
4/6	18:30	69.8	68.2	70.0	68.7	69.7	68.0	69.3	68.4
4/6	18:45	69.6	68.6	70.1	69.1	69.4	68.0	69.3	68.3
4/6	19:00	70.4	68.9	70.8	69.6	70.2	68.6	70.2	69.1
4/6	19:15	70.3	69.2	70.8	69.8	70.3	69.4	70.2	69.5
4/6	19:30	69.8	68.3	70.2	68.7	69.3	67.9	69.4	68.3
4/6	19:45	69.8	68.8	70.4	69.3	69.9	69.0	69.7	68.8
4/6	20:00	69.5	68.5	70.3	69.0	69.7	68.6	69.6	68.9
4/6	20:15	69.8	68.6	70.4	69.3	69.6	68.5	69.4	68.7
4/6	20:30	69.3	68.5	69.6	68.7	69.5	68.4	69.2	68.7
4/6	20:45	69.9	68.7	70.2	69.2	69.4	68.5	69.2	68.5
4/6	21:00	68.8	68.0	69.6	68.6	69.5	68.7	69.2	68.7
4/6	21:15	69.9	68.9	70.3	69.5	69.9	68.8	69.7	69.0
4/6	21:30	69.4	68.4	69.8	68.8	69.3	68.3	69.0	68.7
4/6	21:45	69.7	68.7	70.0	69.3	69.4	68.4	69.1	68.6
4/6	22:00	69.3	68.3	70.0	69.5	69.4	68.7	69.2	68.7
4/6	22:15	69.7	68.7	70.1	69.3	69.5	68.4	69.3	68.7
4/6	22:30	70.3	68.8	70.6	69.6	70.3	68.7	70.1	69.1
4/6	22:45	70.3	69.3	70.8	69.9	70.3	69.4	70.2	69.6
4/6	23:00	70.2	68.8	70.5	69.5	70.2	68.6	70.1	68.9
4/6	23:15	69.5	68.6	70.2	69.4	69.9	68.9	69.5	69.2
4/6	23:30	69.7	68.2	69.9	68.9	69.6	68.0	69.7	68.6
4/6	23:45	70.1	68.8	70.5	69.2	69.7	68.8	69.7	69.0
5/6	0:00	69.3	68.4	70.1	69.2	69.9	68.9	69.6	68.9
5/6	0:15	70.0	68.7	70.3	69.2	69.5	68.7	69.4	68.6
5/6	0:30	69.7	68.8	70.3	69.6	69.8	68.9	69.9	69.1
5/6	0:45	69.0	68.4	70.0	69.0	69.5	68.4	69.0	68.3
5/6	1:00	69.0	68.1	69.7	69.1	69.4	68.7	69.2	68.7
5/6	1:15	69.8	69.0	70.4	69.7	69.9	69.1	69.9	69.2
5/6	1:30	69.9	69.0	70.4	69.8	70.0	69.2	69.9	69.3
5/6	1:45	69.8	69.0	70.4	69.6	69.8	69.0	69.7	69.1
5/6	2:00	69.6	68.5	70.0	69.3	69.4	68.4	69.5	68.7
5/6	2:15	69.9	68.7	70.2	69.5	69.6	68.5	69.8	68.8
5/6	2:30	70.3	69.0	70.9	69.7	70.4	69.1	70.2	69.2
5/6	2:45	70.0	69.0	70.5	69.8	69.9	68.9	69.9	69.1
5/6	3:00	70.4	68.9	71.0	69.6	70.4	69.0	70.2	69.1
5/6	3:15	70.1	69.1	70.8	69.9	70.2	69.4	70.2	69.4
5/6	3:30	70.1	68.7	70.6	69.5	70.1	68.6	69.9	68.9
5/6	3:45	70.1	69.1	70.7	69.8	70.3	69.3	70.2	69.5
5/6	4:00	70.2	69.0	70.6	69.8	70.3	69.2	70.1	69.2
5/6	4:15	70.0	69.0	70.6	69.8	70.2	69.1	69.9	69.1
5/6	4:30	69.8	68.8	70.4	69.6	69.9	68.9	69.7	69.0
5/6	4:45	69.7	68.9	70.3	69.6	69.9	69.0	69.8	69.1
5/6	5:00	69.7	68.9	70.4	69.6	69.9	69.0	69.8	69.1
5/6	5:15	69.9	69.0	70.5	69.8	69.9	69.1	69.8	69.1
5/6	5:30	69.8	68.9	70.4	69.7	69.9	69.1	69.8	69.2
5/6	5:45	69.6	68.8	70.2	69.6	69.6	68.7	69.5	68.8
5/6	6:00	73.6	74.4	73.9	74.1	73.8	74.5	74.1	74.1
5/6	6:15	70.0	69.0	70.5	69.7	70.1	69.1	70.0	69.5
5/6	6:30	69.9	68.5	70.4	69.4	69.9	68.3	69.6	68.7
5/6	6:45	70.1	68.9	70.8	69.7	70.2	69.2	69.9	69.1
5/6	7:00	69.6	68.4	70.1	69.3	69.7	68.5	69.8	68.8
5/6	7:15	60.7	59.4	61.0	63.2	62.5	62.4	59.6	57.8
5/6	7:30	54.0	56.0	59.9	61.2	59.3	60.3	61.1	59.0
5/6	7:45	51.2	51.2	57.4	58.0	55.1	55.5	58.3	53.4
5/6	8:00	42.2	46.1	48.0	54.5	47.5	53.9	50.2	50.7
5/6	8:15	40.1	29.8	41.9	36.0	38.4	34.6	44.8	37.4
5/6	8:30	36.4	25.2	40.2	32.5	40.3	22.2	38.1	24.4
5/6	8:45	33.9	24.8	40.4	33.6	39.1	24.4	35.6	25.0
5/6	9:00	33.9	23.0	38.1	32.3	36.5	22.0	37.1	23.7
5/6	9:15	19.4	19.0	21.0	20.6	20.3	19.1	25.1	18.6













B.3.2 Sample length, sawn orientation and template reference.

Sample #	Length (mm)	Template Ref. (Centre)		Orientation Q, B, or T
		Butt (@)	Top (^)	
648	5100	-	-	T
661	4900	-	-	B
693	4800	-	-	B
615	6100	-	-	B
504	2700	-	-	T
387	3700	-	-	B
598	6100	-	-	B
468	3100	-	-	B
646	4900	-	-	B
669	3700	-	-	T
628	3400	-	-	B
603	3600	-	-	B
697	4800	-	-	B
624	3300	-	-	B
681	4900	-	-	B
581	3700	-	-	T
250	3800	-	-	B
446	3100	-	-	T
382	3100	-	-	T
630	6100	-	-	B
622	4900	-	-	B
679	4800	-	-	B
579	3700	-	-	B
447	3000	-	-	T
445	3100	-	-	B
314	3900	-	-	T
330	3900	-	-	T
475	3100	-	-	B
438	5200	-	-	T
413	3600	-	-	T
433	3000	-	-	T
357	3400	-	-	T
356	3300	-	-	B
269	3000	-	-	B
328	3700	-	-	B
281	2800	-	-	B
218	2800	-	-	T
259	5100	-	-	B
295	4900	-	-	T
248	4800	-	-	T
209	4900	-	-	B
251	5100	-	-	B
289	4900	-	-	B
99	3300	-	-	T
111	3000	-	-	Q
112	3000	-	-	B
143	5200	-	-	B
205	4900	-	-	B
308	5200	-	-	T
95	2400	-	-	B
76	3700	-	-	B
77	3000	-	-	T
68	3400	-	-	B
20	3300	-	-	B
29	3300	-	-	T
27	4800	-	-	T
30	3400	-	-	T
23	3400	-	-	B
848	4900	-	-	T
929	3400	-	-	B
927	3700	-	-	T
852	3700	I30	I4	B
666	3300	A26	E12	B
741	2700	B21	D14	B
850	3600	L8.5	L26.5	B
796	3100	H5.5	G29.5	B
728	2700	F34	F2	Q
1040	5200	H16.5	H20.5	B
966	3300	H31	G31.5	T
1001	3700	ILLEGIBLE	J32.5	B
1039	2800	H5.5	I31.5	T
979	3000	E9	I27.5	B

1007	3000	H22	E14.5	B
1032	5200	H34	G3	B
1025	5200	F33	F5	B
1009	5400	B33	E4	Q
901	5400	-	-	B
845	5400	-	-	B
896	3100	-	-	B
764	4800	O16	?	B
729	5500	B1	A1	T
745	5500	H25.5	G9.5	T
978	4900	I3	H32.5	T
747	5500	H31	H4.5	T
759	3900	L30	ILLEGIBLE	T
832	5500	H13	I25.5	B
734	5100	E16	B24	B
708	5100	A17	A35	B
812	3100	H1	F35	T
993	3000	H27	H9	T
1016	3000	E3.5	H31	Q
707	4300	H13	J23	B
704	4300	F2	G32	B
783	3700	G18	H17	T
841	3600	K12	K23	B
991	3000	H33	I.5	B
1012	3300	I33	I5	B
1347	4900	-	-	T
1348	4900	-	-	B
1341	5100	-	-	T
1006	3000	G2	I32	T
966	3000	K9	M26	B
1196	3300	L5	J28	T
1049	4800	H16	H19.5	B
1242	4800	B2	A1	B
1248	5500	H3	G33	B
1189	5500	C11	A28	B
1145	5500	J13	I22.5	T
1168	3700	E21	E15	T
1153	4300	O23.5	J11	Q
1142	3400	B15	D21	B
1158	3400	D5	D29	B
1133	3400	I27	I11	B
1141	4400	I33.5	I2	B
1100	3700	I19	J15	B
1046	5100	J34.5	I1	B
1172	4900	J8	J25	B
1048	5200	D6	ILLEGIBLE	B
1118	4800	I33.5	I1	T
1159	4300	I9	K26.5	B
1160	3400	G16	H20.5	B
822	3200	-	-	B
1123	3000	-	-	T
1122	3000	-	-	T
1104	5500	-	-	B
1333	5100	-	-	B
1115	5500	-	-	B
1109	5500	-	-	B
1117	5500	-	-	T
1044	5200	C27	A12	B
1053	4900	A3	A30	Q
1058	4800	I30	H4.5	B
1061	5200	F6	A28	B
1063	5200	J2	G34	T
1074	4800	C22	G14	B
1312	5500	K6	K29	B
730	4800	K2	K0	B
988	4800	E5	F30	T
855	5200	ILLEGIBLE	H15	B
1083	2800	I26	H11	T



## Appendix C. Dry Stock Appraisal Data

### A.4. Site 1

#### A.2.5. Species 1

Species 1 25mm Sample #	Uncorrected MC (%)			Corrected MC (%)				Individual Quality Classes Assuming Target MC of 12%	
	Average	Gradient		Average	Gradient			Average	Gradient
	MC <sub>1/3</sub>	MC <sub>1/6</sub>	MC <sub>1/2</sub>	MC <sub>1/3</sub>	MC <sub>1/6</sub>	MC <sub>1/2</sub>	Difference		
1	10	9.5	10.5	11	10.5	11.5	1	A	A
2	14	13.5	16	15	14.5	17	2.5	B	B
3	13	13	14	14	14	15	1	A	A
4	15	14.5	16	16	15.5	17	1.5	C	A
5	11	11	11	12	12	12	0	A	A
6	14	13	14	15	14	15	1	B	A
7	17	16	19	18	17	20	3	E	B
8	13	13	14	14	14	15	1	A	A
9	14	13.5	15	15	14.5	16	1.5	B	A
10	15	15	17	16	16	18	2	C	A
11	10.5	10	11	11.5	11	12	1	A	A
12	11	11	12	12	12	13	1	A	A
13	11.5	11	12.5	12.5	12	13.5	1.5	A	A
14	10.5	10.5	11	11.5	11.5	12	0.5	A	A
15	10.5	10	11	11.5	11	12	1	A	A
16	9.5	9.5	10	10.5	10.5	11	0.5	A	A
17	13	13	13.5	14	14	14.5	0.5	A	A
18	12	11.5	12	13	12.5	13	0.5	A	A
19	13	12.5	13.5	14	13.5	14.5	1	A	A
20	11	10	11	12	11	12	1	A	A
21	13	13	15	14	14	16	2	A	A
22	12	11.5	12.5	13	12.5	13.5	1	A	A
23	9.5	9	10	10.5	10	11	1	A	A
24	11	11	11.5	12	12	12.5	0.5	A	A
25	12.5	12	13	13.5	13	14	1	A	A
26	9.5	9	10	10.5	10	11	1	A	A
27	9.5	9	9.5	10.5	10	10.5	0.5	A	A
28	10	10	10.5	11	11	11.5	0.5	A	A
29	11	11	12	12	12	13	1	A	A
30	9.5	9	9.75	10.5	10	10.75	0.75	A	A
31	11	10.5	12	12	11.5	13	1.5	A	A
32	9	8.5	9	10	9.5	10	0.5	A	A
33	10.5	10	11	11.5	11	12	1	A	A
34	10	10	10.5	11	11	11.5	0.5	A	A
35	10	9	10	11	10	11	1	A	A
36	9	8	9.5	10	9	10.5	1.5	A	A
37	12	11.5	12.5	13	12.5	13.5	1	A	A
38	9	8.5	9	10	9.5	10	0.5	A	A
39	8	8	8.5	9	9	9.5	0.5	B	A
40	9	8.5	9.5	10	9.5	10.5	1	A	A

<b>Overall 90% Class</b>	<b>B</b>	<b>A</b>
--------------------------	----------	----------

A.2.6. Species 2

Species 2	Uncorrected MC (%)			Corrected MC (%)				Individual Quality Classes	
	25mm	Average	Gradient	Average	Gradient			Assuming Target MC of 10%	
Sample #	MC <sub>1/3</sub>	MC <sub>1/6</sub>	MC <sub>1/2</sub>	MC <sub>1/3</sub>	MC <sub>1/6</sub>	MC <sub>1/2</sub>	Difference	Average	Gradient
1	7.5	7.5	8	8	8	8	0	B	A
2	10	9.5	10	9	9	9	0	A	A
3	9	9	10	9	9	9	0	A	A
4	8	7.5	10	8	8	9	1	B	A
5	8	8	9	8	8	9	1	B	A
6	10.5	10.5	12.5	9.5	9.5	10.5	1	A	A
7	10	10	11	9	9	10	1	A	A
8	9.5	9	10	9	9	9	0	A	A
9	11	11	13	10	10	11	1	A	A
10	11	11	12.5	10	10	10.5	0.5	A	A
11	9	8.5	10	9	8.5	9	0.5	A	A
12	9	9	10	9	9	9	0	A	A
13	10	10	11	9	9	10	1	A	A
14	9	9	10	9	9	9	0	A	A
15	8.5	8.5	10	8.5	8.5	9	0.5	A	A
16	10	9.5	11.5	9	9	10	1	A	A
17	7	7	8	8	8	8	0	B	A
18	9	8.5	10.5	9	8.5	9.5	1	A	A
19	10.5	10.5	13	9.5	9.5	11	1.5	A	B
20	11.5	11.5	15	10	10	12	2	A	B
21	10	10	11.5	9	9	10	1	A	A
22	9.5	9.5	10	9	9	9	0	A	A
23	10	10	11.5	9	9	10	1	A	A
24	10.5	10.5	12	9.5	9.5	10	0.5	A	A
25	12	11.5	13	10	10	11	1	A	A
26	11.5	11.5	13	10	10	11	1	A	A
27	10.5	10.5	12.5	9.5	9.5	10.5	1	A	A
28	10	10	12	9	10	10	0	A	A
29	11	11	12	10	10	10	0	A	A
30	9	8.5	9.5	9	8.5	9	0.5	A	A
31	9.5	9.5	11	9	9	10	1	A	A
32	10.5	10.5	12	9.5	9.5	10	0.5	A	A
33	10	10	11.5	9	9	10	1	A	A
34	10	10	11	9	9	10	1	A	A
35	9.5	9.5	11	9	9	10	1	A	A
36	11	11	12	10	10	10	0	A	A
37	11	11	12.5	10	10	10.5	0.5	A	A
38	10	9.5	10.5	9	9	9.5	0.5	A	A
39	12	11.5	13	10	10	11	1	A	A
40	12	12	13.5	10	10	11.5	1.5	A	B

<b>Overall 90% Class</b>	<b>A</b>	<b>A</b>
--------------------------	----------	----------

A.5. Site 2

B.2.3. Species 1

Species 1 25mm Sample #	Uncorrected MC (%)			Corrected MC (%)				Individual Quality Classes Assuming Target MC of 12%	
	Average	Gradient		Average	Gradient			Average	Gradient
	MC <sub>1/3</sub>	MC <sub>1/6</sub>	MC <sub>1/2</sub>	MC <sub>1/3</sub>	MC <sub>1/6</sub>	MC <sub>1/2</sub>	Difference		
1	9.2	9	9.5	11.2	11	11.5	0.5	A	A
2	18	15	20	20	18	22	4	F	C
3	10.4	9.8	11	13.4	11.8	14	2.2	A	B
4	10.2	9.6	11	13.2	11.6	14	2.4	A	B
5	11	10	12	14	13	15	2	A	A
6	8.8	8.6	9	10.8	10.6	11	0.4	A	A
7	9.6	9.4	9.4	11.6	11.4	11.4	0	A	A
8	10.2	9.8	10.4	13.2	11.8	13.4	1.6	A	A
9	10	9.8	9.6	13	11.8	11.6	-0.2	A	A
10	9	8.6	9.2	11	10.6	11.2	0.6	A	A
11	15	14.2	16	18	17.2	18	0.8	E	A
12	11.6	11	12.4	14.6	14	15.4	1.4	B	A
13	13	12.2	14	16	15.2	17	1.8	C	A
14	12.4	11	13.2	15.4	14	16.2	2.2	B	B
15	12.2	11.4	13.2	15.2	14.4	16.2	1.8	B	A
16	10.6	9.4	11.2	13.6	11.4	14.2	2.8	A	B
17	10	9.4	10.2	13	11.4	13.2	1.8	A	A
18	14.2	12.2	15	17.2	15.2	18	2.8	E	B
19	9.8	9.4	10	11.8	11.4	13	1.6	A	A
20	11.2	10.2	12.4	14.2	13.2	15.4	2.2	B	B
21	13	11.6	13.8	16	14.6	16.8	2.2	C	B
22	11.2	10.4	12	14.2	13.4	15	1.6	B	A
23	12.2	11.6	12.2	15.2	14.6	15.2	0.6	C	A
24	10.2	9.2	11	13.2	11.2	14	2.8	A	B
25	13	12	13.8	16	15	16.8	1.8	C	A
26	11	10.4	11	14	13.4	14	0.6	B	A
27	12.2	10.8	14	15.2	13.8	17	3.2	C	C
28	10.4	9	11.6	13.4	11	14.6	3.6	A	C
29	12.2	11.6	13.4	15.2	14.6	16.4	1.8	C	A
30	12.2	11.6	12.8	15.2	14.6	15.8	1.2	C	A
31	12.8	11.8	13.6	15.8	14.8	16.6	1.8	C	A
32	10.8	9.6	12	13.8	11.6	15	3.4	A	C
33	12.4	11.4	13.4	15.4	14.4	16.4	2	C	A
34	11.2	10.4	12	14.2	13.4	15	1.6	B	A
35	10.4	10	10.4	13.4	13	13.4	0.4	A	A
36	9.8	9.4	10	11.8	11.4	13	1.6	A	A
37	11.4	10.4	12	14.4	13.4	15	1.6	C	A
38	9.6	9.2	9.8	11.6	11.2	11.8	0.6	A	A
39	11.2	10.8	11.8	14.2	13.8	14.8	1	C	A
40	9.8	8.8	10.6	11.8	10.8	13.6	2.8	A	B

<b>Overall 90% Class</b>	<b>C</b>	<b>B</b>
--------------------------	----------	----------

B.2.4. Species 2

Species 2 25mm	Uncorrected MC (%)			Corrected MC (%)				Individual Quality Classes Assuming Target MC of 12%	
	Average	Gradient		Average	Gradient			Average	Gradient
Sample #	MC <sub>1/3</sub>	MC <sub>1/6</sub>	MC <sub>1/2</sub>	MC <sub>1/3</sub>	MC <sub>1/6</sub>	MC <sub>1/2</sub>	Difference	Average	Gradient
1	14.4	13	14.6	17.4	16	17.6	1.6	E	A
2	13.2	11.8	14	16.2	14.8	17	2.2	D	B
3	15.4	12.8	17	18.4	15.8	19	3.2	F	C
4	14.4	12.6	15.4	17.4	15.6	18.4	2.8	E	B
5	16.2	13.6	17.6	18.2	16.6	19.6	3	F	B
6	14.6	13.2	14.8	17.6	16.2	17.8	1.6	E	A
7	14	11.8	15.2	17	14.8	18.2	3.4	E	C
8	15.4	13.2	16.2	18.4	16.2	18.2	2	F	A
9	16.2	13	17.6	18.2	16	19.6	3.6	F	C
10	14.2	12.2	15.2	17.2	15.2	18.2	3	E	B
11	15	13.4	15.2	18	16.4	18.2	1.8	E	A
12	15.2	12.4	16.4	18.2	15.4	18.4	3	F	B
13	14.6	12.6	16	17.6	15.6	18	2.4	E	B
14	16	13.2	17.2	18	16.2	19.2	3	E	B
15	16	14.2	16.2	18	17.2	18.2	1	E	A
16	16	16	15	18	18	18	0	E	A
17	16	14.8	16.2	18	17.8	18.2	0.4	E	A
18	15.6	14.2	16	18.6	17.2	18	0.8	F	A
19	18	16	18	20	18	20	2	F	A
20	16	13	16	18	16	18	2	E	A
21	18	16	18.2	20	18	20.2	2.2	F	B
22	14.2	12.6	14.4	17.2	15.6	17.4	1.8	E	A
23	17.4	14.6	18	19.4	17.6	20	2.4	F	B
24	17	15	14.4	19	18	17.4	-0.6	F	A
25	16.2	13.2	16.8	18.2	16.2	18.8	2.6	F	B
26	16.2	12.6	17.6	18.2	15.6	19.6	4	F	C
27	17.2	13.6	18.2	19.2	16.6	20.2	3.6	F	C
28	15	12.4	16	18	15.4	18	2.6	E	B
29	17.8	13	20	19.8	16	22	6	F	E
30	15	12.6	17	18	15.6	19	3.4	E	C
31	14.2	12.8	14.2	17.2	15.8	17.2	1.4	E	A
32	15	13.2	16	18	16.2	18	1.8	E	A
33	14.2	13.2	14.4	17.2	16.2	17.4	1.2	E	A
34	14.8	14	15.8	17.8	17	18.8	1.8	E	A
35	15.6	14	16	18.6	17	18	1	F	A
36	16	15	16	18	18	18	0	E	A
37	15.6	14.2	16	18.6	17.2	18	0.8	F	A
38	15.2	14.2	15	18.2	17.2	18	0.8	F	A
39	16.2	15.6	16	18.2	18.6	18	-0.6	F	A
40	15.2	14	16	18.2	17	18	1	F	A

<b>Overall 90% Class</b>	<b>F</b>	<b>C</b>
--------------------------	----------	----------

A.6. Site 3

C.3.1. Species1

Species 1 25mm Sample #	Uncorrected MC (%)			Corrected MC (%)				Individual Quality Classes Assuming Target MC of 10%	
	Average MC <sub>1/3</sub>	Gradient MC <sub>1/6</sub> MC <sub>1/2</sub>		Average MC <sub>1/3</sub>	Gradient MC <sub>1/6</sub> MC <sub>1/2</sub> Difference			Average	Gradient
1	7.5	7	7.5	8.5	8	8.5	0.5	B	A
2	8	7.5	8	9	8.5	9	0.5	A	A
3	7.5	7	8	8.5	8	9	1	B	A
4	7.5	7.5	8	8.5	8.5	9	0.5	B	A
5	8	8	9	9	9	10	1	A	A
6	8.5	8.5	9	9.5	9.5	10	0.5	A	A
7	7.5	7	7.5	8.5	8	8.5	0.5	B	A
8	8	7.5	8	9	8.5	9	0.5	A	A
9	8	7.5	8	9	8.5	9	0.5	A	A
10	7.5	7	8	8.5	8	9	1	B	A
11	7.5	7.5	8	8.5	8.5	9	0.5	B	A
12	7	7	7	8	8	8	0	B	A
13	7.5	7.5	8.5	8.5	8.5	9.5	1	B	A
14	7.5	7	8.5	8.5	8	9.5	1.5	B	A
15	7	7	9	8	8	10	2	B	B
16	7	6.5	7.5	8	7.5	8.5	1	B	A
17	7	7	9.5	8	8	10.5	2.5	B	C
18	8	7.5	8.5	9	8.5	9.5	1	A	A
19	7.5	7.5	9	8.5	8.5	10	1.5	B	B
20	7.5	7	9	8.5	8	10	2	B	B
21	7	7	8	8	8	9	1	B	A
22	6.5	6.5	7.5	7.5	7.5	8.5	1	C	A
23	7	6.5	7.5	8	7.5	8.5	1	B	A
24	7	7	7.5	8	8	8.5	0.5	B	A
25	8	8	9	9	9	10	1	A	A
26	7	6.5	7.5	8	7.5	8.5	1	B	A
27	7.5	7.5	8.5	8.5	8.5	9.5	1	B	A
28	7.5	7.5	10	8.5	8.5	11	2.5	B	C
29	9	9	10.5	10	10	11.5	1.5	A	A
30	8	8	9.5	9	9	10.5	1.5	A	A
31	9	8.5	10	10	9.5	11	1.5	A	A
32	7	7	8	8	8	9	1	B	A
33	7.5	7.5	10	8.5	8.5	11	2.5	B	C
34	8.5	8	10	9.5	9	11	2	A	B
35	7	7	8	8	8	9	1	B	A
36	7.5	7	9	8.5	8	10	2	B	B
37	8	8	10	9	9	11	2	A	A
38	7	6.5	7	8	7.5	8	0.5	B	A
39	7	7	8	8	8	9	1	B	A
40	11.5	11	12	12.5	12	13	1	B	A

<b>Overall 90% Class</b>	<b>B</b>	<b>B</b>
--------------------------	----------	----------

C.3.2. Species 2

Species 2 25mm Sample #	Uncorrected MC (%)			Corrected MC (%)				Individual Quality Classes Assuming Target MC of 10%	
	Average	Gradient		Average	Gradient			Average	Gradient
	MC <sub>1/3</sub>	MC <sub>1/6</sub>	MC <sub>1/2</sub>	MC <sub>1/3</sub>	MC <sub>1/6</sub>	MC <sub>1/2</sub>	Difference		
1	7.5	7	8	8	8	8	0	B	A
2	7	6.5	9	8	7.5	9	1.5	B	B
3	7	7	8.5	8	8	8.5	0.5	B	A
4	8	7.5	10	8	8	9	1	B	A
5	8	8	12	8	8	10	2	B	B
6	8	7.5	9.5	8	8	9	1	B	A
7	7	6.5	8	8	7.5	8	0.5	B	A
8	8	8	12	8	8	10	2	B	B
9	6.5	6	7	7.5	7	8	1	C	A
10	13	12.5	14	11	10.5	12	1.5	A	B
11	7	6.5	7	8	7.5	8	0.5	B	A
12	8	8	12	8	8	10	2	B	B
13	8	7.5	9	8	8	9	1	B	A
14	7	6.5	7.5	8	7.5	8	0.5	B	A
15	11	11	13	10	10	11	1	A	A
16	7.5	7	9	8	8	9	1	B	A
17	8.5	8.5	14	8.5	8.5	12	3.5	B	D
18	8	8	12	8	8	10	2	B	B
19	16	15	16	13	12	13	1	B	A
20	14	13.5	15	12	12	12	0	A	A
21	16	15	17	13	12	13	1	B	A
22	8.5	8.5	13	8.5	8.5	11	2.5	B	C
23	7	6.5	7	8	7.5	8	0.5	B	A
24	7	7	10	8	8	9	1	B	A
25	8	7.5	10	8	8	9	1	B	A
26	11	11	14	10	10	12	2	A	B
27	14	13.5	14.5	12	12	12	0	A	A
28	13	13	14.5	11	11	12	1	A	A
29	14	13.5	14.5	12	12	12	0	A	A
30	13	13	15	11	11	12	1	A	A
31	10	9	11	9	9	10	1	A	A
32	14.5	14	16	12	12	13	1	A	A
33	8	8	12	8	8	10	2	B	B
34	7	6.5	8.5	8	7.5	8	0.5	B	A
35	9	9	13	9	9	11	2	A	B
36	12.5	12	13	10	10	11	1	A	A
37	8	8	11.5	8	8	10	2	B	B
38	10.5	10	12.5	9	9	10.5	1.5	A	B
39	13	12.5	15	11	10.5	12	1.5	A	B
40	12	11	13	10	10	11	1	A	A

<b>Overall 90% Class</b>	<b>B</b>	<b>B</b>
--------------------------	----------	----------

A.7. Site 4

C.4.1. Species 1

Species 1 25mm Sample #	Uncorrected MC (%)			Corrected MC (%)				Individual Quality Classes Assuming Target MC of 10%	
	Average MC <sub>1/3</sub>	Gradient MC <sub>1/6</sub> MC <sub>1/2</sub>		Average MC <sub>1/3</sub>	Gradient MC <sub>1/6</sub> MC <sub>1/2</sub> Difference			Average	Gradient
1	9	8.5	9.5	10	9.5	10.5	1	A	A
2	8.5	8.5	9	9.5	9.5	10	0.5	A	A
3	9	8.5	9	10	9.5	10	0.5	A	A
4	9	8.5	9	10	9.5	10	0.5	A	A
5	9	9	9.5	10	10	10.5	0.5	A	A
6	8	7.5	8.5	9	8.5	9.5	1	A	A
7	8.5	8	9	9.5	9	10	1	A	A
8	9.5	9.5	10	10.5	10.5	11	0.5	A	A
9	8	8	9	9	9	10	1	A	A
10	8.5	8.5	9	9.5	9.5	10	0.5	A	A
11	8.5	8	9	9.5	9	10	1	A	A
12	9	9	9	10	10	10	0	A	A
13	8.5	8	8.5	9.5	9	9.5	0.5	A	A
14	8	8	8.5	9	9	9.5	0.5	A	A
15	9	8.5	9	10	9.5	10	0.5	A	A
16	9	8.5	9.5	10	9.5	10.5	1	A	A
17	8	8	8.5	9	9	9.5	0.5	A	A
18	9.5	9	9.5	10.5	10	10.5	0.5	A	A
19	9	9	9.5	10	10	10.5	0.5	A	A
20	9.5	9	10	10.5	10	11	1	A	A
21	9.5	9	10	10.5	10	11	1	A	A
22	9	8.5	9	10	9.5	10	0.5	A	A
23	9	9	9	10	10	10	0	A	A
24	9	9	9.5	10	10	10.5	0.5	A	A
25	9	8.5	9	10	9.5	10	0.5	A	A
26	8.5	8	9	9.5	9	10	1	A	A
27	8	8	8.5	9	9	9.5	0.5	A	A
28	9	9	10	10	10	11	1	A	A
29	9	8.5	9.5	10	9.5	10.5	1	A	A
30	9	8.5	9	10	9.5	10	0.5	A	A
31	9	9	9.5	10	10	10.5	0.5	A	A
32	8.5	8.5	10	9.5	9.5	11	1.5	A	B
33	8.5	8	9	9.5	9	10	1	A	A
34	10	10	10	11	11	11	0	A	A
35	10	10	10.5	11	11	11.5	0.5	A	A
36	10	9.5	10.5	11	10.5	11.5	1	A	A
37	9.5	9	9.5	10.5	10	10.5	0.5	A	A
38	9	9	9.5	10	10	10.5	0.5	A	A
39	9	8.5	9	10	9.5	10	0.5	A	A
40	10	9.5	10.5	11	10.5	11.5	1	A	A

<b>Overall 90% Class</b>	<b>A</b>	<b>A</b>
--------------------------	----------	----------

C.4.2. Species 2

Species 2	Uncorrected MC (%)			Corrected MC (%)				Individual Quality Classes	
	25mm	Average	Gradient	Average	Gradient			Assuming Target MC of 10%	
Sample #	MC <sub>1/3</sub>	MC <sub>1/6</sub>	MC <sub>1/2</sub>	MC <sub>1/3</sub>	MC <sub>1/6</sub>	MC <sub>1/2</sub>	Difference	Average	Gradient
1	9.5	9	11	9	9	10	1	A	A
2	10	9	10	9	9	9	0	A	A
3	10	9.5	11	9	9	10	1	A	A
4	10	9	10.5	9	9	9.5	0.5	A	A
5	10	9	11	9	9	10	1	A	A
6	8.5	8.5	9	8.5	8.5	9	0.5	B	A
7	10	9.5	10.5	9	9	9.5	0.5	A	A
8	10.5	10	11	9.5	9	10	1	A	A
9	12	11	12.5	10	10	10.5	0.5	A	A
10	9.5	9.5	10.5	9	9	9.5	0.5	A	A
11	10	10	10.5	9	9	9.5	0.5	A	A
12	9.5	9	10	9	9	9	0	A	A
13	10.5	10	11.5	9.5	9	10	1	A	A
14	9.5	9	10	9	9	9	0	A	A
15	9.5	9	10	9	9	9	0	A	A
16	10	10	10.5	9	9	9.5	0.5	A	A
17	10	10	11	9	9	10	1	A	A
18	10.5	10	12	9.5	9	10	1	A	A
19	10	10	11	9.5	9	10	1	A	A
20	9.5	9	10	9	9	9	0	A	A
21	9	9	10	9	9	9	0	A	A
22	10	9.5	10.5	9	9	9.5	0.5	A	A
23	9.5	9	10	9	9	9	0	A	A
24	10.5	10	12	9.5	9	10	1	A	A
25	12	11.5	13	10	10	11	1	A	A
26	10	9.5	11	9	9	10	1	A	A
27	10	10	10.5	9	9	9.5	0.5	A	A
28	11	10.5	12	10	9.5	10	0.5	A	A
29	10.5	10	11	9.5	9	10	1	A	A
30	11	10.5	12	10	9.5	10	0.5	A	A
31	9.5	9	10	9	9	9	0	A	A
32	11	11	13	10	10	11	1	A	A
33	11	10.5	12	10	9.5	10	0.5	A	A
34	11	10.5	12	10	9.5	10	0.5	A	A
35	9	8.5	10	9	8.5	9	0.5	A	A
36	10	10	10.5	9	9	9.5	0.5	A	A
37	10	10	11	9	9	10	1	A	A
38	10.5	10	11	9.5	9	10	1	A	A
39	11.5	11	12	10.5	10	11	1	A	A
40	10.5	10	11	9.5	9	10	1	A	A

<b>Overall 90% Class</b>	<b>A</b>	<b>A</b>
--------------------------	----------	----------



A.8. Site 5

C.5.1. Species 1

Species 1 25mm Sample #	Uncorrected MC (%)			Corrected MC (%)				Individual Quality Classes Assuming Target MC of 12%	
	Average MC <sub>1/3</sub>	Gradient MC <sub>1/6</sub> MC <sub>1/2</sub>		Average MC <sub>1/3</sub>	Gradient MC <sub>1/6</sub> MC <sub>1/2</sub> Difference			Average	Gradient
1	10.1	8	12.5	13.1	10	15.5	5.5	A	E
2	10.9	9.1	12.4	13.9	11.1	15.4	4.3	A	D
3	10.1	8.1	12.1	13.1	10.1	15.1	5	A	D
4	11	9.3	13.5	14	11.3	16.5	5.2	A	E
5	10.9	9.2	13	13.9	11.2	16	4.8	A	D
6	10.1	8.4	12	13.1	10.4	15	4.6	A	D
7	10.2	8.5	12.2	13.2	10.5	15.2	4.7	A	D
8	10.1	7.9	12.3	13.1	9.9	15.3	5.4	A	E
9	10	8.1	12	13	10.1	15	4.9	A	D
10	10	9.1	12	13	11.1	15	3.9	A	C
11	10.9	9.8	12.8	13.9	11.8	15.8	4	A	D
12	9	8.3	10.1	11	10.3	13.1	2.8	A	B
13	10.4	9.5	11.8	13.4	11.5	14.8	3.3	A	C
14	8.4	8	8.9	10.4	10	10.9	0.9	A	A
15	8	7.9	8	10	9.9	10	0.1	A	A
16	8.4	8	8.5	10.4	10	10.5	0.5	A	A
17	9.6	7.9	11.3	11.6	9.9	14.3	4.4	A	D
18	9.8	8.5	11	11.8	10.5	14	3.5	A	C
19	9.8	9	11.5	11.8	11	14.5	3.5	A	C
20	11	8.5	13	14	10.5	16	5.5	A	E
21	8.5	8	9.2	10.5	10	11.2	1.2	A	A
22	9.3	9	8.8	11.3	11	10.8	-0.2	A	A
23	9.7	8	11.4	11.7	10	14.4	4.4	A	D
24	10	8.3	12	13	10.3	15	4.7	A	D
25	9.5	8	11.2	11.5	10	14.2	4.2	A	D
26	10.6	9	12.2	13.6	11	15.2	4.2	A	D
27	10.8	9	13	13.8	11	16	5	A	D
28	10.4	8.5	12.2	13.4	10.5	15.2	4.7	A	D
29	9.2	7.4	11.2	11.2	9.4	14.2	4.8	A	D
30	10	9.2	12	13	11.2	15	3.8	A	C
31	11	9.9	11.8	14	11.9	14.8	2.9	A	B
32	9	8.3	10	11	10.3	13	2.7	A	B
33	11.2	10.8	12.1	14.2	13.8	15.1	1.3	B	A
34	12	11.2	12.1	15	14.2	15.1	0.9	B	A
35	10.6	10	11.4	13.6	13	14.4	1.4	A	A
36	11	10.2	11	14	13.2	14	0.8	A	A
37	11	10.5	11.8	14	13.5	14.8	1.3	A	A
38	10.8	10	12	13.8	13	15	2	A	A
39	10.5	10	11	13.5	13	14	1	A	A
40	12	11.3	12	15	14.3	15	0.7	B	A

<b>Overall 90% Class</b>	<b>A</b>	<b>D</b>
--------------------------	----------	----------